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TRACE-D USERS' MANUAL

JULY 1969

S. G. Santarelli

Prepared for

DIRECTORATE OF PLANNING AND TECHNOLOGY

ELECTRONIC SYSTEMS DIVISION
AIR FORCE SYSTEMS COMMAND
UNITED STATES AIR FORCE
L. G. Hanscom Field, Bedford, Massachusetts



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Project 7070
Prepared by
THE MITRE CORPORATION
Bedford, Massachusetts
Contract F19628-68-C-0365

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FOREWORD

This report was prepared by The MITRE Corporation for the Directorate of Planning and Technology, Electronic Systems Division, Air Force Systems Command, L.G. Hanscom Field, Bedford, Massachusetts, under Contract F19628-68-C-0365.

REVIEW AND APPROVAL

Publication of this technical report does not constitute Air Force approval of the report's findings or conclusions. It is published only for the exchange and stimulation of ideas.

ANTHONY P. TRUNFIO
Technical Advisor
Development Engineering Division
Directorate of Planning and Technology

ABSTRACT

This report describes the MITRE version of the TRACE-D program now in operation. While the primary function of TRACE-D is orbit determination, options are also available in the program for trajectory prediction and observational data generation. A functional description of these features is contained in this report along with a complete user's manual and a brief program description.

PREFACE

The program described herein is a modified version of the TRACE-D program originally developed by the Aerospace Corporation in Los Angeles. Although the modifications made were many and included conversion of the program to FORTRAN IV and STRAP, restructuring of the program logic, and the addition of minor options and features, the basic functions (i.e., orbit determination, trajectory prediction, and observational data generation) remain intact.

The people involved in various aspects of the effort, in addition to the uthor, were Dr. K. K. Maitra, G. M. Hyder, P. E. Shifres, and S. Schwartz. A great deal of appreciation is due to K. W. Hubbard, C. C. Tonies, and other members of the Flight Mechanic's Department of the Aerospace Corporation whose cooperation in obtaining the program and unlimited assistance throughout the task were invaluable.

This report is intended solely as a user's guide to the TRACE-D program, and therefore contains only a brief functional description of the analytics. For the reader seeking the mathematical details and arguments the ideal reference is the original document issued by the Aerospace Corporation (see [1]).

Material from this Aerospace document has been freely incorporated into this report wherever pertinent and is not to be taken as original.

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Section 1.

BASIC INFORMATION

1.1 Introduction

This document is intended as a user's manual and therefore does not discuss the theory and mathematical details of TRACE-D except in a functional context. Section 1 of this report presents some program history, a brief summary of the modification process, and a statement of the program's present status. Section 2 specifies the functional capabilities of TRACE-D while Sections 3 and 4 describe input and output (patterned after the original TRACE-D document) and Section 5 contains programming information. Wherever pertinent, throughout the report, material from the Aerospace documentation has been freely incorporated.

1.2 Program History

The TRACE-D orbit determination program was developed by the Aerospace Corporation as a multipurpose, flexible computational tool for application to problems in orbit analysis. A major design objective was that the program be able to provide answers to a wide range of problems relating to orbit and system design, space vehicle performance, and force model analysis. It was not and is not a "real time" program and therefore it is most effective for post-flight analysis and also for research and investigative purposes. The program has been used extensively and successfully by the staff at Aerospace in just such an environment.

TRACE-D was originally written in FORTRAN II and FAP for use on the IBM 7094 computer in the "CHAIN" multi-coreload mode of operation. About thirty-percent of the program consisted of machine language (FAP) subroutines including the numerical integration package. The status of the program at the time of its release to us was reported to be operational for all functions.

1.3 Modification Process

The primary objective of this effort was to produce a version of TRACE-D operable on the IBM 7030 computer here at MITRE. To accomplish this, two separate yet simultaneous endeavors were carried out; one being to get the original TRACE-D program to run successfully on a nearby 7094 installation, and the other the actual conversion of routines to FORTRAN IV and STRAP and the reconstruction of the program. Upon completion of this phase, the next step was the checkout and "debugging" of the 7030 version of the program. This task was greatly facilitated and accelerated by running test cases for all options with both versions (7094 and 7030) of TRACE-D and checking all results.

I ring accomplished the primary objective satisfactorily, work began on minor adjustments and additions to the program. Such features as observation residual plotting, an expanded earth geopotential capability, and a dynamic constraint matrix capability for site location adjustments were implemented. At the present time the program is operational on the 7030 computer and has produced meaningful and significant results for many MITRE orbit-related problems.

Section 2.

MAJOR PROGRAM FUNCTIONS

2.1 Trajectory Prediction

Basic to all the functions of the TRACE-D program is the generation of a time history (either in a forward or backward direction; see Section 3) of the position and velocity of a space vehicle in an inertial frame of reference. However, this inertial ephemeris as well as its associated ground track and altitude history are, in many instances, of interest in themselves. Thus, these computations are performed and printed out in the trajectory prediction mode of TRACE-D.

The motion of a space vehicle is generated by numerical integration of the appropriate differential equations of motion. Using a Cowell formulation (i.e., expressing the total acceleration vector as three components in a cartesian system $[\ddot{x}, \ddot{y}, \ddot{z}]$) three non-linear second-order differential equations are derived. A predictor-corrector numerical integration procedure based on "eighth-order differences" is used to obtain position (x, y, z) and velocity $(\dot{x}, \dot{y}, \dot{z})$ at any time to based on the known position and velocity at some initial time t_0 .

The total acceleration vector, mentioned above, is actually a sum of the effects of the perturbing forces that comprise the TRACE-D dynamic model. The earth geopotential effects (gravity) are included in the form of a spherical harmonic expansion with provision for zonal harmonics J_2 through J_{15} and all tesseral and sectorial terms through J_{15} , J_{15} . Effects due to other bodies in the solar system (Sun, Moon, Venus, Mars, Jupiter) are computed from inverse-square law formulas and positions of the other bodies are obtained from tabulated coordinates stored on magnetic tape (planetary tape). Acceleration due to atmospheric drag is assumed to be directly proportional to the square of the velocity of the vehicle relative to the air. The atmospheric density is obtained from one of two different

model atmospheres that are incorporated into the program according to the user's choice. Instantaneous changes in the inertial velocity vector may be applied at specific times to simulate maneuvers such as orbit adjust or vehicle separation. Also, an included low-thrust acceleration term may be used to simulate thrust tailoff in cases involving large engines, long-term constant thrust, or, in some instances, leaking tanks or valves.

Although all of the above effects are programmed into the TRACE-D equations of motion, the actual model that is employed may include some, all, or none of these perturbations. The user has the option to choose the model by setting a series of indicators. The comparative 1sting of associated input and output quantities given in Table 1 suggests the range of potential application. Complete instructions for preparation of trajectory mode input data and a sample of a typical trajectory mode output listing are given in Sections 3 and 4.

2.2 Observation Generation

The object of the data generation function is to generate various forms of simulated measurements from a given definition of the ephemeris of a vehicle and the location of observing stations on the earth's surface. These measurements may be any of twenty different types from up to one hundred different sites and may be generated at userspecified frequencies. Both "clean" and "noisy" data are available, the latter being generated by adding noise of specified variances and biases to the "clean" measurements. Upon user request, the visibility function (i.e., the rise and set times) of a vehicle with respect to one or more stations may be obtained without printout of any intermediate data. When data is generated, it may be written on magnetic tape or punched on cards and is formatted such that it is readily available as input to the orbit determination process.

This option lends itself well to many applications, two of which are the following: studies of the effects of specific data imperfections

on orbit determination convergence behavior and the fitting of data using a different force model than that used to generate the data giving insight into the real-world problem of fitting live data with programmed (and always less than perfect) dynamic models.

Since the calculations performed for this option encompass all the calculations of the trajectory prediction mode, the input quantities include all those listed in Table 1 plus the additional information in Table 2. Available output quantities are listed in Table 2 also, but a more specific list of available data types with definitions is included in Sections 3 and 4.

2.3 Orbit Determination

Orbit determination is the primary function of the TRACE-D program and encompasses both the trajectory prediction and observation generation modes. Stated in simplest form the orbit determination problem consists of extracting information from observations (possible 20 types) of a space vehicle. The data is generally collected by a network of tracking stations on the surface of the earth. Nearly always, the information to be extracted includes the orbital elements but may include many other parameters of the dynamic model and of the tracking system.

The process of extraction in TRACE-D takes the form of a generalized least-squares differential correction procedure. More specifically,
the goal is to determine values for a set of parameters (from the dynamic and/or observational model) such that the differences between
the actual input measurements and corresponding values computed from
the model (usually termed observation residuals) will be minimized in
a least-squares sense. The solution set may be comprised of not more
than one hundred parameters, of which not more than sixty may be trajectory-related parameters (i.e., initial conditions, geopotential
coefficients, etc.). The amount of data that may be fitted is restricted only by the nature of the problem and not by the program.

Table 1. Input/Output Quantities Associated with TRACE-D Trajectory Mode

	Input Data			Output Data
2. 1.	Earth-model constants Atmosphere model constants		1.	Satellite inertial position and velocity in rectangular and spherical coordinates
<u></u>	Solar system constants		2.	Magnitudes of geocentric-radius and inertial-velocity vectors.
4.	Units conversion factors		3,	Latitude and longitude of sub-vehicle point
5.	Numerical integration-control constants		. 4	Altitude above earth
6.	Epoch time Position and velocity or orbital elements at epoch time	Items Printed Out	*. ~	Differences between two trajectories in rectangular, spherical, classical element, and orbit-plane coordinates
<u> </u>	Satellite ballistic	regular Time Intervals	*.9	Time difference between corresponding points of two trajectories
6	Time, magnitude, and direction of velocity increments		7.*	Magnitudes of distance and velocity difference vectors for two trajectories
*	* Associated with a trajectory differencing	rencing		

Table 1 (cont.)

	Input Data			Output Data
10.	Interval, amplitude, and decay rate of low thrust	,	* * * * * * * * * * * * * * * * * * * *	Partial derivatives of trajectory position with respect to differential-equation parameters
11.	Table of time points where output is to occur Parameter selection indicators		****	Differences between changes in position and velocity produced by perturbing parameters and changes predicted by corresponding calculated partial derivatives
13.	Tape-unit numbers for			
14.	trajectory differencing Latitudes and longitudes		10.	At time when vehicle crosses as- cending node:
	are to occur	Items Printed Out at Special Time Points		Output Items I through 4 above Classical orbital elements Mean and true anomaly Nodal regression rate Rate of advance of the line of apsides Apogee and perigee radius
				Keplerian, anomalistic, and nodal periods
* *	Refer to the partial derivatives	of trajectory po	osition	derivatives of trajectory position with respect to selected parameters.

Table 1 (cont.)

Input Data			Output Data
15. Minor option indicators		10.	(continued)
<u>P</u>	Items Printed Out at Special		Revolution number (this set obtained Nodal period by simple differ-Nodal regression than by formula)
E.	Time Points	11.	At time of the event
			Orbit adjust magnitude and direction Magnitude of low thrust at start and stop times and at ascending node times
		12.	At the time when the flight path angle passes through ninety degrees (roughly at apogee and perigee):
	9		Output Items 1 through 4 above
		13.	At the time when the vehicle reaches local maximum or minimum altitude (when h = 0):
			Output Items 1 through 4 above

Table 2.

Input/Output Quantities Associated with
TRACE-D Observation Generation Mode

INPUT DATA

- 1. All input listed in Table 1.
- 2. Site location coordinates
- 3. Visibility function indicator
- 4. Observation types
- 5. Observation frequencies
- 6. Noise information
- 7. Output mode (card, tape)
- 8. Refraction specifications
- 9. Uncertainty matrix for adBARV at epoch

- OUTPUT DATA
- 1. Computed observations
- Rise-set times (per station)
- *3. Observation uncertainties

^{*} Is the propagation and effect of input 9 above.

In fact, TRACE-D is capable of fitting observational data from six vehicles in a single orbit determination procedure. It allows for estimation of the trajectory initial conditions and drag coefficients associated with five satellites in addition to the usual parameters in a single satellite run.

The list of all possible input for the orbit determination mode is quite extensive as can be seen from Table 3. This is, of course, due to the comprehensive model programmed into TRACE-D for the purpose of wider and more varied applications. However, flexibility has not been sacrificed for completeness, so that the program is easily adaptable to either a non-real or more-real environment by simple input adjustment. The input and output capabilities of orbit determination are listed in Table 3 and described in detail in Sections 3 and 4. Table 4, which follows, is a complete list of all possible parameters that may be differentially corrected in TRACE-D.

Table 3. Input/Output Associated with Orbit Determination Mode

OUTPUT

12. Tape of residuals

INPUT

12. Tape specifications

1.	All input in Table 1.	1.	Chronological list of all observations by satellite
2.	Parameters in solution set	2.	Variational equation solutions
3.	Initial conditions for satellites 2-6	3.	Trajectory printouts
4.	Bounds for parameter correction	4.	Observation partial derivatives
5.	Station locations	5.	Residuals
6.	Data errors and biases	6.	Station and observation type RMS summary
7.	Data editing criterion	7.	Computed and predicted RMS
8.	Refraction correction indicators	8.	Corrections
9.	Iteration count	9.	Covariance matrix
10.	Constraint matrix for parameters	10.	Correlation matrix
11.	Observations from all vehicles	11.	Solution set

Table 4.

Parameter List*

- 1. Initial position and velocity components in either spherical, rectangular, or classical element form for up to six independent space vehicles.
- 2. Reciprocal of ballistic coefficients for up to six different satellites.
- 3. Up to six velocity increments (KICKS) for one satellite.
- 4. Amplitude and time constant for an exponentially decaying low thrust.
- 5. Zonal harmonic coefficients J_2 through J_{10} and all tenseral harmonics $J_{2,1}$ through $J_{6,6}$.
- 6. Constant biases on all types of observations.
- 7. Scale factors for range and range-rate observations.
- 8. Time biases (i.e., biases in reported times at which observations were made).
- 9. Latitudes, longitudes and altitudes above sea level of observing stations.
- * On any one run up to 100 of listed quantities may comprise the solution set with not more than 60 from types 1-5.

Section 3.

Usage

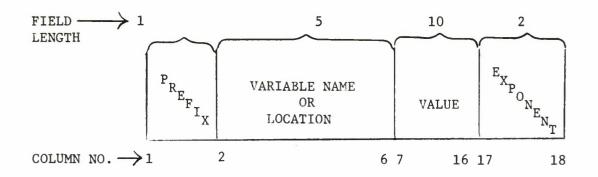
3.1 Preliminary Facts

In order to run the TRACE-D program the user need not concern himself with the internal elements of the program or worry about handling a cumbersome deck of cards. The entire program is stored on tape and can be used simply by attaching an appropriate data deck to the small basic running deck supplied by MITRE and submitting the job for execution. The basic running deck contains only tape usage information and the necessary instructions to trigger execution, therefore it is never necessary for the user to alter it in any way. Due to the varied tape requirements for each of the major functions, there are three versions of the basic running deck and the appropriate one must be used for each option exercised.

The input to the TRACE-D program falls into two categories: one which follows the normal FORTRAN IV rules of input and the other which is interpreted by a special routine in the program. The former method is used for all observing-station data (only a fraction of total input) and needs no description, while the latter method is used for all remaining input and requires a brief explanation.

The input routine accepts each piece of data from a data card in a field of eighteen columns in length with four distinct subfields as shown on the following page.

¹ The user who is curious or interested in the actual programming facts will find these concisely presented in Section 5.



1. <u>Prefix Field</u> - The prefix field is one column in length and can occupy columns 1, 19, 37, or 55. The mode of the input that follows is dictated by what is punched (or not punched) in the prefix field. The following are the permissible prefixes.

Prefix	<u>Data-Modes</u>
blank	Floating point number, number contains or implies a decimal point.
I	Fixed point number, no decimal point.
D	Hollerith information, data is not a number but a sequence of characters which can extend into the exponent field.
G	Used in connection with integra- tion parameters, basic constants and the earth model. It indicates that card contains a symbolic name followed by a comment.
Н	Followed by 1 or 2 in column 2. This is simply a header card to be printed at various places on the output. The number 1 indicates columns 1-80 and 2 indicates columns 81-132 on the printout.

2. <u>Location Field</u> - The location field is 5 columns in length and starts in columns 2, 20, 35 and 56. The information punched in the location field is either a symbolic name or a subscript. A symbolic

name defines a location in core where the data is stored. In the case of a subscript, it is used with respect to the immediately preceding symbolic name. Therefore, whenever a symbolic name is the name of a table, a subscript of 1 is attached to that name and those subscripts greater than 1 indicate storage relative to the start of the table. All names and subscripts should be left-adjusted within the field.

- 3. <u>Value Field</u> The value field, 10 columns in length, starts in columns 7, 25, 43, or 61. This field together with the exponent field contains the numerical or hollerith data which is to be input. In the event the data is an integer (prefix = I) the exponent field is ignored. If the data is a floating point number (prefix column is blank, not punched) the decimal point, whenever it is not punched within the value field, is assumed to be after the last digit. Whenever hollerith data is input (prefix = D) the exponent field becomes an <u>extension</u> of the value field thus allowing for a total of twelve characters in the hollerith quantity. All data in the value field must be left-adjusted.
- 4. Exponent field The exponent field, two columns in length, starts in columns 17, 35, 53, and 71. This field allows for a range of floating point numbers from 10^{-19} to 10^{-99} . An exponent of 10 or smaller must start with the letter J (i.e., $J\emptyset = -10$, J5 = -15, etc.). As in the value field the characters in the exponent field must be left-adjusted.

Although the input routine will accept four input fields per card, it is not necessary to use all four. One field used per card is just as correct since the rest of the card is ignored.

In addition to the precise field format there are a few other rules of input preparation.

- 1. The actual order of the data cards is <u>almost</u> immaterial, the only restriction being that all values with subscripts in the location field are placed in the input deck relative to the last previous symbolic name.
- 2. Any input which does not apply to the immediate run or is to have

a value of zero need not be specified.

- 3. In the case of two appearances of the same location symbol, the last one to appear defines the effective input.
- 4. The basic input units are feet, degrees, and seconds. Therefore, whenever the units are not stated then they are a combination of the basic set.

With the preceding basic description and the details on input preparation that follow, the user should have sufficient knowledge to use the TRACE-D program successfully.

3.2 Basic Data

The .erm "basic data" is defined as the data that is common to all the principal TRACE-D functions. This includes the constants for the integration procedure, the necessary physical constants, function indicator, trajectory specifications (like epoch time, initial conditions) and force model inputs.

3.2.1 Constants

The constants constitute two lengthy lists of input and involve quite a bit of keypunching. Because of this, there is available a standard set, in card deck form, which may be used as is, or altered for specific entries. This facility reduces the user's card preparation time and eliminates possibility of error.

In the event that the constants must be punched they must be formatted as shown on the following page.

3.2.1.1 Lines 1 - 19 Standard Set of Integration Constants¹

LINE # PREFIX				EXPONENT	
	Cols. 1,19,37,55	Cols. 2,20,38,56	Cols. 7,25,43,61	Cols. 17,35,53,71	
1	G	INTEG			
2	I	1	1		
3	I	2	2		
2 4	I	4	1		
5	I	5	1		
6		11	1.00002516		
7		23	1.	10	
8		26	1.		
9		30	1.		
10		31	.015625		
11		32	64.		
12		33	1.	- 7	
13	I	34	4		
14	I	35	1		
15	I	36	0		
16		37	.001		
17		38	0.		
18		40	2820.1763		
19	I	41	1		

¹ For definitions of the constants consult Table 5.

² Notice that there are entries missing in the INTEG list, like the 3rd one, for instance. This is because these entries are either not necessary for all options or are used by the program and not available to the user. This is true in both constants lists.

3.2.1.2 Lines 20 - 46 Standard Set Physical Constants 1

LINE #	PREFIX	NAME OR SUBSCRIPT	VALUE	EXPONENT
	Cols. 1,19,37,55	Cols. 2,20,38,56	Cols. 7,25,43,61	Cols. 17,3 5 ,53,71
20	G	С		The state of the s
21		1	.43752691	- 2
22		2	.55303935	- 2
23		6	.5	
24		8	.43752691	- 2
25		9	1.	
26		13	3280.8399	
27		14	57.2957795	
28		15	20925738.	
29		16	332951.3	
30		17	.0122999	
31		18	.814979	
32		19	.107821	
33		20	317.887	
34		21	95.129	
35		22	23454.865	
36		23	3443.9336	
37		24	20925738.	
38		25	348762.3	
39		26	32.174	
40		30	348762.3	
41		31	1.5	
42		32	1.0471976	
43		33	3.14159265	
44		34	298.3	
45		35	300000.	
46		36	82505.922	*

 $^{^{\}mathrm{1}}$ For definitions of constants consult Table 5.

Table 5.

INTEG and C Constants Lists

INTEG	PA	RAMETERS OF THE TRAJECTORY INTEGRATION
1	1	Formulation. 1 - Cowell (eqs. of motion), 2 - Encke
		(note: the Encke-T formulation is presently not
		available)
2	2	Differential equation subroutine. 1 - AMRK, 2 - COW
3		angle in degrees for changing mean to true equinox
4	1	Sun (4-9) are selectors for other-body perturbations
5	1	Moon If tape unit number at numb(18) is not zero,
6	0	Venus the perturbations are included or omitted
7	0	Mars according as the selector is non-zero or zero
8	0	Jupiter
9	0	Saturn
10	C(22)	Sun (10-15) are interpolation scale factors for use
	- ()	using contents of C(22), the number of earth-radii
11	1.00002516	Moon in an astronomical unit:
12	C(22)	Venus
13	C(22)	Mars
14	C(22)	Jupiter
15	C(22)	Saturn
16	0	Similar velocity scale factors. (not now used, and
thru	a ara sun i arase allu-	all zero).
21	0	
22	Ŭ	(used internally - Encke)
23	IE-10	E Bar, COW subroutine truncation error control para-
		meter.
24		(used internally - Encke)
25		(used internally - Encke)
26	1.	A, see COW writeup.
27-29		(not used)
30	1.	Initial time step size.
31	.015625	
32	64.	Maximum time step size
33		Kepler equation convergence criterion.
34	4	Ratio of Cowell step size to Runge-Kutta step size
35	i	if 1, do not recompute perturbations for corrector.
33	-	if 2, do.
36		Flag for perturbation computation
30		(used if INTEG(35) = 1).
37	.001	Least squares convergence criterion (relative)
38	. 001	Least squares convergence criterion (absolute)
39	. 0	(not used)
40	2820.1763	Speed of light (earth-radii/minute)
41	2020.1703	If non-zero, round position and velocity vectors
71	1	for acceleration computation. If zero, truncate
		Tot acceleration computation. It zero, cluncate

Table 5 (cont.)

INTEG	PARAMETERS OF THE TRAJECTORY INTEGRATION				
42	Reserved for later use				
C CONS					
1	.0043752691	Earth rotation rate (rad/min)			
2	.0055303935	Gm, earth gravitation constant (ER**3/min**2)			
3		Option for speed of light correction			
4		B=1-E, relative semi-minor axis of ellipsoid			
_		(computed in CSET)			
5		B**2/A**2 = (1-E)**2 (computed in CSET)			
6	.5	Factor for decreasing bounds in L. S. solution			
7		2*E-E**2 (computed in CSET)			
8	.0043752691	Atmosphere rotation rate (rad/min)			
9	1.	Earth radius			
10		Input N for N-sigma residual editor			
11		Input scale factor for N-sigma residual editor			
12		If input non-zero, go thru 1st iteration twice			
		for sums			
13	3280.8399	Feet/kilometer			
14	57.2957795	Angle conversion factor			
15	20925738.	A, earth radius in feet			
16	332951.3	Relative mass of sun			
17	.0122999	Moon			
_18	.814979	Venus			
19	.107821	Mars			
20	317.887	Jupiter			
21	95.129	Saturn			
22	23454.865	Earth-radii/astronomical unit			
23	3443.9336	Nautical miles (6076.1155 ft)/earth radius			
24	20925738.	I/O distance conversion factor			
25	348762.3	I/O velocity conversion factor			
26	32.174	Go (used for CDA/W and thrust/W)			
27		Input parameter difference for trajectory			
		differencing			
28		Input threshold for percent difference for			
		trajectory differencing			
29		Constant for doppler rate			
_30	348762.3	Ft/sec per Er/min -			
31	1.5	Factor for increasing bounds in L. S. solution			
32	1.0471976	Rad/min per deg/sec			
_33	3.14159265	PI			
34	298.3	Reciprocal of E = ellipticity			
35	300000.	Critical altitude (ft)			
36	82505.922	Deg/day per rad/min			
37-39		Direction cosines of body axis for look angle			

3.2.2 Functions to be Performed

LINE #

				 , ¹
47	D	ITIN	1234	

Line 47 contains the ordered list of all functions to be performed during a single run. Selection of functions is governed in accordance with the following code numbers.

Code numbers

Functions

12 ---- Orbit Determination

4 ----> Data Generation

Up to twelve functions may be selected in any one run, i.e., the program will perform twelve specified functions in one continuous machine job. The example above specifies that an orbit determination be carried out first followed by a trajectory prediction and then a data generation.

3.2.3 <u>Trajectory Specifications</u>

3.2.3.1 <u>Lines 48-54 Epoch</u>

48	I	YEAR	1963	
49	I	MNTH	6	
50	I	DAY	15	
51		TZNE	0	
52		HR	12	
53		MIN	45	
54		SEC	15.5	

Please notice that the field labels are no longer specified (i.e., Prefix, Value, etc.) but they are, of course, implied by the divisions.

In the usual case, wherein the year, month, and day are input with the year positive, the X-axis is directed to the vernal equinox. Alternatively, if the year is input negative, the X-axis would be directed to the longitude of Greenwich. The hour, minute, and second entries refer to midnight of zone time. Greenwich Mean Time is Time Zone 0.

3.2.3.2 Lines 55-61 Initial Conditions

I	ICTYP	2
	IC	126.1
	2	31.23
	3	89.
	4	14.
	5	22600114
	6	25117.3
	I	I ICTYP

Line 55 indicates which of the ten IC types (1, 2, ..., 9, 0) are entered in Lines 56 through 61. The alternative ICTYP entries are characterized as follows:

- a. IC Type 1 Earth-centered inertial cartesian coordinates $(x, y, z, \dot{x}, \dot{y}, \dot{z} \text{ in units of feet and feet per second})$ (see Section 3.1.1.1).
- b. IC Type 2 Spherical coordinates (α, δ, β A, R, v) in units of degrees, feet, and feet per second (see Section 3.1.1.2). In Line 14, negative r is interpreted as height above the earth's surface in feet. In Line 15, if v is negative, cifcular velocity is computed and used.
- c. IC Type 3 Orbital elements (a, e, i, Ω , ω , τ) in units of feet, degrees, and minutes (see Section 3.1.1.3).
- d. IC Type 4 Same as Item b above, with longitude $\,\lambda\,$ replacing right ascension $\alpha.$
- e. IC Type 5 No IC's input. The last trajectory point of the immediately preceding case is used.
- f. IC Type 6 No IC's input. The corrected initial conditions from the last previous tracking run are used.

- g. IC Type 8 Either Type 1 or 2 above, but in units of earth radii, minutes, and radians. Type number is entered at CPRAM (see Section 5.1.2.2).
- h. IC Type 9 Same as Type 1 above, but in units of earth radii and earth radii per minute.
- i. IC Type 0 No IC's input. For a tracking run, two R, A, E sets are used from the data to calculate a set of initial conditions (see Section 3.6.6).

3.2.4 Force Model Inputs

3.2.4.1 Lines 62-68 Drag and T Matrix

62		DRAG	.01
63	I	2	1
64		4	
65		4	
66		6	-8.6
67		7	-55.5
68	I	TMATX	4

Line 62 contains the drag parameter CDA/W in square feet per pound and Line 63 contains the atmosphere model specification (ARDC 59 or Lockheed/ Jacchia). The ARDC model will be used when DRAG(2) is 0 and the Lockheed/Jacchia model when DRAG (2) is 1. If line 63 is a 1, Lines 64 and 65 contain quantities used in the Lockheed/Jacchia model.

Lines 64 and 65 contain d_1 and d_2 , respectively. These are values of certain constants in the Lockheed-Jacchia atmospheric density expressions. (Consult reference 1 for details).

An entry in Line 68, TMATX, will cause the T matrix (the 3×3 matrix describing the dependence of drag force upon vehicle position) to be used in the variational equations in accordance with the following options:

- a. TMATX = 0 T matrix is not used.
- b. TMATX = 1 Input $\partial \rho / \partial h$ is used with no earth flattening.
- c. TMATX = 2 Input $\partial \rho / \partial h$ is used with earth flattening.
- d. TMATX = 3 $\partial \rho / \partial h$ is calculated with no earth flattening.
- e. TMATX = 4 $\partial \rho / \partial h$ is calculated with earth flattening.

Also, with TMATX non-zero, Lines 66 and 67 should contain input values for $\partial \rho/\partial h$. Lines 66 and 67 contain $\partial \rho/\partial h$ for altitudes between 76 and 108 n. mi. and between 108 and 376, respectively.

It showd be noted that input values for $\partial \rho/\partial h$ must be used with the ARDC 1959 model. If a variable C_D term is desired, the drag table option may be utilized. In this case, the drag parameter may be considered to consist of the product of two terms, $(C_DA/W) \times C_D^{\dagger}$, wherein C_DA/W is a constant which can be differentially corrected by the use of the variational equation and C_D^{\dagger} may be considered a function of Mach number below a certain altitude and as a function of altitude at points above that altitude. Alternatively, C_D^{\dagger} may be considered a function of time. In either case, use of the drag table is necessary.

When the drag table is not used, input of C_DA/W into the DRAG location does not change usual TRACE operation. In this case, C_D^{\dagger} is automatically set equal to 1. If the drag table is used, the following additional inputs are required:

- a. DRAG(10) If DRAG(10) = 0, tables not used. If DRAG(10) = 1, Mach and altitude tables used.
 - If DRAG(10) = 2, time table only used.
- b. DRAG(11) Altitude above which altitude table is used and below which Mach table is used $(needed\ if\ (DRAG(10) = 1).$
- c. DRAG(12) = 0 Used by interpolation routine.

DRAG(13) Altitude table, or time table if through (35) DRAG(10) = 2 (h₁, C'_D(h₁), h₂, C'_D(h₂) . . . , h_n, C'_D(h_n), 0, 0, or
$$t_1, C'_D(t_1), t_2, C'_D(t_2), . . . , t_n, C'_D(t_n), 0, 0).$$

d. DRAG(36) = 0 Used by interpolation routine.

DRAG(37) Mach table (stored as noted in Item c. through (59) above).

3.2.4.2 <u>Lines 69-75</u> Other Body Perturbations

68 II	I	CTAPE	l 7 l	

If perturbations due to other bodies in the solar system are to be included in the trajectory calculations, a planetary coordinate tape must be mounted and the logical-tape unit number 7 must be entered at CTAPE.

69	G	С		
70	I	4	1	
71	I	5	1	
72	I	6	0	
73	I	7	0	
74	I	8	0	
75	I	9	0	

Lines 69-75 contain the C constants that indicate which bodies are being considered. The six bodies corresponding to C(4) through C(9) are the Sun, Moon, Venus, Mars, Jupiter, and Saturn. Entering a 1 in C(4) implies that the Sun is to be considered, while entering a 0 in C(9) implies that Saturn is ignored. Therefore, in the example above only the Sun and Moon are used in the other-body perturbation computation.

3.2.4.3 Lines 76-79 Exponential Thrust

76	THRST	
77	2	
78	3	
79	4	

If an exponential thrust is to be used, the quantities T_1 in units of force/mass = ft/sec², T_2 in units of min⁻¹, and t_s and t_f in seconds from midnight of epoch date must be input at THRST, THRST(2), THRST(3), and THRST(4) locations, respectively.

3.1.4.4 Lines 80-96 Gravity Perturbations

80	I	IFLAG		
81	I	28	Ø	

Lines 80 and 81 above contain the input quantity $IFLAG(28) = \emptyset$. This is an indicator that must be set in order to clear storage for the earth model that is to be specified.

82	I	IOB	10	
83	I	2	6	
84	I	3	1Ø	
85	I	4	6	

Lines 82-85 define the number of terms to be used in the earth geopotential expansion. IOB(1) is the number of zonals and IOB(2) is the index of tesserals. Therefore, in the example above, 10 zonals will be used and tesseral terms up to and including the 6,6 term. Lines 84 and 85 specify IOB(3) and (4) which are the number of terms to be used in the V-matrix. The V-matrix is a measure of the dependence of the gravitational force upon vehicle position and is included as one of the many necessary calculations for the observation

partial derivatives (for differential correction).

If these two values are set to zero the V-matrix calculations are ignored. For a derivation of the V-matrix and its implications Appendix B of Reference 1 is recommended.

86	OBJZ		
87	2	1,826	-2
88	3	2,485	-6

Lines 86-88 specify the zonal coefficients in the following order:

	11		·	1
89		OBJT		
90		2 "	1.556	-6
91		3	2.26	-6
92		4	1.72	-6
93		OBLT		
94		2	16.18	
95		3	35.62	
96		4	108.2	

Lines 89-96 specify the tesseral coefficients and the lambdas to be used, in the following order:

OBJT	J_{nm}	OBLT	τ_{nm}
(1)	J_{21}	(1)	τ21
(2)	J_{22}	(2)	τ22
(3)	J ₃₁	(3)	τ31
(4)	J ₃₂	(4)	τ32
(5)	J ₃₃	(5)	τ33
(6)	J_{41}	(6)	J ₄₁
e	etc.	et	c.

3.2.5 <u>Miscellaneous Inputs</u>

3.2.5.1 Lines 97-100 Instantaneous Orbit Adjusts

97	PKICK	89020.31		
98	2	200.		
99	3	0		
100	4	62.		
		**		
	_			

Instantaneous orbit adjusts are input at PKICK. Line 97 contains t_1 (time of first orbit adjust, OA_1) in seconds from midnight of epoch; Line 98 contains K (magnitude of velocity change of OA_1) in feet per second; Line 99 contains θ (yaw angle for OA_1) in degrees, and Line 100 contains θ_D (pitch angle for OA_1) in degrees.

The TRACE-D program will accommodate up to six orbit adjusts. Additional cards may be added as necessary for $0A_2$ through $0A_6$.

3.2.5.2 <u>Lines 101-107</u> <u>Extra Kicks</u>

101	I	NXK	3
102		XKICK	63456
103		2	.2
104		3	88721
105		4	10.
106		5	101018
107		6	.02

Up to fifty fixed orbit adjusts (i.e., instantaneous changes of the in-track velocity component) may be input at XKICK. It should be noted that these orbit adjusts are not parameters for differential correction, but are applied in the equations of motion only and are independent of the PKICK inputs. The number of extra kicks (\leq 50) is input at NXK, and the table of times and ΔV values is input beginning at XKICK. The format is time, ΔV , time, ΔV , etc., in units of seconds from midnight of epoch day and feet per second, respectively.

3.2.5.3 Line 108 Print Code

									_					
100	1 20	DDCDE	1	2	2	1.		C .	7	0	0	1 1 1	11	10
1 108 1	1 1) (PKUDE	I I	L 2		14	1 0		/	1 0	19	LIU	1 1 1	1 12
1 -00			_	_	_		_			_				
1	1													

The print-code entry consists of two BCD words accommodating six character positions each. Entry of an X at any of these twelve positions will initiate corresponding outputs in accordance with the following:

- a. (1) Trajectory (trajectory only option).
- b. (2) Residuals (tracking only option).
- c. (3) Partials (tracking only option).
- d. (4) $A^{T}A$ after each iteration (tracking only option).
- e. (5) Variational equations (trajectory only option).

- f. (6) Orbital elements (trajectory only option).
- g. (7) Do not print station locations (tracking and data generation).
- h. (8) Not used.
- i. (9) Special trajectory prints¹
- j. (10) Orbital elements at ascending nodes only (trajectory only option).
- k. (11) Not used.
- (12) Suppress all trajectory print except ascending nodes (trajectory only option)²

3.2.5.4 Line 109 Equinox Precession Corrections

109	DALFG	.0002

The rotational position of the earth with respect to the inertial system is characterized by the right ascension of Greenwich at midnight on the day of epoch (α_g) and is computed with respect to the mean equinox of epoch date. An additional factor for correcting to true equinox of epoch date optionally may be input at DALFG in units of degrees.

3.2.5.5 Lines 110-113 Direction of Integration

The TRACE-D program is capable of generating a time history of position and velocity in a forward or backward direction in any one run.

The inputs which determine this direction are INTEG(30), INTEG(31), INTEG(32). If these inputs are negative then backward integration from epoch time is assumed by the program. If positive,

Prints will occur at times of maximum and minimum altitude above the oblate earth, at times when the flight-path angle equals 90 degrees and at special latitudes and longitudes if values are entered (see Section 3.3.6).

² If the option to write a binary trajectory tape (B7) has been selected, the writing of that tape is controlled by the PRTIM entries (see Section 3.3.1).

as in the standard case, forward integration from epoch is performed.

110	G	INTEG	
111	30		-1.
112	31		01
113			-10.

The example shown above indicates to the program that backward integration must be performed starting at epoch with an initial time step of -1. minute (see Table 5 for the explanation of INTEG constants), a minimum time step of -.01 minutes and a maximum time step of -10. minutes.

When performing any of the three basic options, these inputs may be set negative. In trajectory generation a time history back from epoch will be produced. In the observation generation mode, observations previous to epoch may be generated. In the orbit determination mode, data previous to epoch may be fit. Generally this makes TRACE-D a more flexible program by making the position of epoch and the known initial conditions less rigid.

It should be noted that both backward and forward integration can not be performed in the same run but two runs would have to be made, each with a different direction of integration.

3.2.5.6 Line 114 Primary Scratch Tape

11/	т	PTAPE	/.
114		FIAFE	4

PTAPE is the number of the primary scratch tape that the program requires and 4 is its only permissible value. This card must be included in every data deck.

3.3 Trajectory-Only Data

In addition to the basic data previously described, the following data is relevant to the trajectory generation.

3.3.1 <u>Lines 1-7 Print Time Vector Option</u>

	1	I	PRTIM	
n	2	I	2	
_t ₀	3		3	
Δt ₁	4		4	
t ₁	5		5	
Δt ₂	6		6	
t ₂	7		7	

The above sequence of print times is for outputs selected by PRCDE entries (Line 108, Section 3.2.5.3). As many as nine sets of print intervals may exist (Line 2). In the case of the i^{th} set, output is from t_{i-1} to t_i at intervals of Δt_i , with all times in minutes from midnight of epoch date if PRTIM = 1 or from epoch if PRTIM = 0. Additional cards may be inserted if $3 \le n \le 9$. It should be noted that a normal print at epoch is automatic.

3.3.2 <u>Lines 8-15</u> <u>Variational Equation Partial Derivatives</u>

								-	=
8	D	CPRAM							
9	D	DPRAM							
10	D	3							
11	D	5							
12	D	7							
13	D	9							
14	D	KPRAM							
15	D	3							
			-	 _		_	_		_

An X entered in any CPRAM, DPRAM, or KPRAM character position causes the corresponding variational equation to be solved. Printout of the partial derivatives will occur only if an X is entered at Character Position 5 in the PRCDE print code entry location. The ordering of entries in the CPRAM, DPRAM, and KPRAM character position boxes is as follows:

a. CPRAM (Initial Condition Parameters) (Line 8)

(TC

The first position specifies which one of three types of initial conditions is applicable, and succeeding positions indicate the particular parameters that are desired in each case. Ordering of CPRAM parameter entries for initial condition (IC) Types 1, 2, and 3 as shown below.

	Type))								
(either)	1	x	у	z	x	ÿ	ż	t ₀		
(or)	2	α	δ	β	A	r	v	t ₀		
(or)	3	а	е	i	Ω	ω	τ	t ₀		

Ordering of CPRAM IC Parameter Entries

b. <u>DPRAM and KPRAM (Differential Equation Parameters)</u> (Lines 9 through 15)

The ordering of DPRAM and KPRAM parameter entries is shown below, wherein T_1 and T_2 are the exponential thrust parameters and a_i , K_i θ_{y_i} , and θ_{p_i} are the OA number (1, 2, ..., 6), ΔV magnitude, yaw angle, and pitch angle, respectively.

Sixty differential equation parameters is the maximum number which may be selected for any one run.

DPRAM	DRAG	ļμ	J ₂	J ₃	J4	J5	J ₆	J7	Jg	Jg	J10	J ₂₁
3	J ₂₂	J _{3.1}	J ₃₂	J ₃₃	1341	J42	J43	J44	J ₅₁	J ₅₂	J ₅₃	J 54
5	J ₅₅	J ₆₁	J ₆₂	J ₆₃	J ₆₄	J ₆₅	J ₆₆	λ2]	122	λ_{31}	λ32	λ33
7	λ41	λ ₄₂	λ ₄₃	λ,,,	۸ 51	λ ₅₂	Å 53	λ ₅₄	[^] 55	λ ₆₁	λ ₆₂	λ63
9	λ64	λ65	λ66		ωa	T_1	T2					

KPRAM	a ₁	K ₁	θy	θ_{p_1}	a ₂	KZ	θ y 2	θ _{p2}	a ₃	К3	θ y 3	θ_{p_3}
3	a_	K 4	θу.,	θ p ₄ ,	a ₅	К ₅	θ y 5	θ _{p5}	a ₆	Κ _Ĝ	θ y 6	θ _{p6}

Ordering of DPRAM and KPRAM Differential Equation Parameter Entries

3.3.3 Lines 16-18 Trajectory Comparison Options

16	I	IDIFF	1	[
17	I	NTAPE	15	
18	I	DTAPE	14	

Tape units and case indicators required for the trajectory differencing function are as follows:

- a. IDIFF = 0 A regular trajectory run is indicated.
- b. IDIFF = 1 The reference trajectory will be written on the logical tape specified by NTAPE. If no entry is input at NTAPE, Logical Tape 15 will be used.
- c. IDIFF = 2 The differences between the present and reference cases are computed and written on the logical tape specified by DTAPE. If no entry is input at DTAPE, Logical Tape 14 will be used. The difference tape specified by DTAPE is rewound at the beginning of the case.
- d. IDIFF = 3 Conditions are the same as when IDIFF = 2 except that the tape specified by DTAPE is not rewound.

- e. IDIFF = 4 The tape specified by DTAPE is rewound at the beginning of the case and unloaded upon completion.
- f. IDIFF = 5 The tape specified by DTAPE is unloaded upon completion of the case.

The significance of the foregoing options is that if a single-comparison case is to be processed, IDIFF = 1 is used for the reference case and IDIFF = 4 for the perturbed case. If a series of perturbed cases are to be processed, IDIFF = 1 is used for the reference case, IDIFF = 2 for the first perturbed case, IDIFF = 3 for all intermediate cases, and IDIFF = 5 for the last perturbed case.

When this option is used, a special running deck must be obtained which defines the necessary tapes specified above.

3.3.4 Line 19 Revolution Number

19 REV	7
--------	---

If an initial value other than zero is desired for the revolution number, it may be input at the REV location. This value must be reinitialized for each individual case.

3.3.5 Line 20 Trajectory Tape Generation

20	I	TTAPE	3	

If TTAPE is non-zero, a binary trajectory tape will be generated on Logical Tape 19 in accordance with the following input options:

- a. TTAPE = 0 Tape will not be generated.
- b. TTAPE = 1 Tape will be rewound before generating but not unloaded after completion. This entry should be used for the first case when more than one case is involved.
- c. TTAPE = 2 Tape will not be rewound before generating and not unloaded after completion. This entry should be used for all intermediate cases.

- d. TTAPE = 3 Tape will be rewound before generating and unloaded after completion. This entry should be used when only one case is involved.
- e. TTAPE = 4 Tape will not be rewound before generating but will be unloaded after completion.

 This entry should be used for the last case.

This tape is not suitable for the trajectory-comparison option of the trajectory-only function.

For this option also, a special running deck containing the proper tape definitions must be used.

3.3.6 <u>Lines 21-28</u> <u>Latitude and/or Longitude Prints</u>

n_1	21	I	LATPR	3
	22		2	10.
	23		3	15.
	24		4	20.
n ₂	25	I	LØNPR	3
n ₂	25 26	I	LØNPR 2	200.
n ₂		I		3
n ₂	26	I		200.

Line 21 contains n_1 ($n_1 \le 10$), or the number of special latitudes at which trajectory prints are requested, and Lines 22 through 24 contain the special latitudes. Additional cards may be added if $4 \le n_1 \le 10$.

Line 25 contains n_2 (n_2 < 10). or the number of special longitudes at which trajectory prints are requested, and Lines 26 through 28 contain the special longitudes. Additional cards may be added if $4 \le n_2 \le 10$.

Note that an X must be entered in Character Position 9 of the PRCDE entry if either of the foregoing options are selected.

This concludes the description of trajectory related data. For data deck samples and running deck setups see Section 3.6.

3.4 Observation Generation Data

The following data is pertinent only to the data generation option and is used in conjunction with the basic data (described in Section 3.3).

3.4.1 <u>Lines 1-4</u> <u>Special Output Option</u>

1		IFLAG	
2	I	6	1

If IFLAG(6) = 0, all generated data are printed. If IFLAG(6) = 1, rise, maximum elevation, and set times only are printed and the Data-Generation Specification Load Sheet II is not necessary except for listing of a card carrying TR in Columns 1 and 2 (see Section 3.4.5 and 3.4.6).

3 1 14			
J 11 1 14 1	3	Т	1/4
	J	1 1	19

If IFLAG(14) = 0, data are generated in time sequence until the available core space (bucket) is full. This output is then separated and printed by station in the same sequence as that of the input station cards. Further data are then generated until the bucket is again full, and the sort/print cycle is repeated. If IFLAG(14) = 1, data are printed as they are generated (i.e., in time sequence).

4	I	ETAPE	6

If ETAPE is non-zero, a BCD radar observation tape will be generated on the logical tape unit entered at ETAPE. The tape format will be the same as that of the tracking input data, including station locations and TF and TR cards.

3.4.2 <u>Lines 5-23</u> <u>Vehicle Attitude Specifications</u>

YAW	1.	
PITCH	90.	
ROLL	180.	
	PITCH	PITCH 90.

Vehicle attitude may be specified by inputting yaw, pitch, and roll angles in degrees in the manner shown above. These entries normally are introduced in conjunction with aspect angle computations.

8	YAW	
9	811	1.
10	812	120.
11	813	.01
12	814	.1
13	815	0
14	816	120.
15	817	121.
16	818	9
17	819	-9.0
18	820	0
19	821	1420.
20	822	1420.5
21	823	360.
22	824	0
23	825	0

The time history of vehicle attitude maneuvers may be specified by means of a table entered at YAW(811). The format of this table, which is used in connection with generation of radar aspect angles and may consist of up to three sets of five entries each, is itemized in Table 6.

The yaw-, pitch-, and roll-angle values that make up these input sets of angular rates are assumed to change at the rate given over the time interval defined by the start and stop times. Nominal orientation is zero yaw, pitch and roll which corresponds to the condition where the vehicle body axis is normal to the geocentric radius vector, the nose of the vehicle is in the in-track direction, and the top of the vehicle is in the direction of the extended radius vector.

Vehicle attitude at time of epoch and for the case where the entries in Table 6 are all zero (i.e., when nothing is input) is assumed to be the attitude specified at YAW, PITCH, and ROLL. If gaps in the time entries of the table are present, the angles are held constant at the last computed values.

Table 6.
YAW(811) TABLE FORMAT

Entry	Description
YAW(811)	Start time in minutes from epoch for first set of angular rates.
YAW(812)	Stop time in minutes from epoch for first set of angular rates.
YAW(813)	Yaw rate in degrees per minute.
YAW(814)	Pitch rate in degrees per minute.
YAW(815)	Roll rate in degrees per minute
YAW(816)	Start time in minutes from epoch for second set of angular rates.
YAW (817)	Stop time in minutes from epoch for second set of angular rates.
YAW(818)	Yaw rate in degrees per minute.
etc.	etc.

3.4.3 Lines 24-38 Data Error Inputs

1					_									
	24	B	NOISE	3	7	7	7	7	7	7	7	7	7	7
-1	1		110101	_	,	,	,	•	_′				L	

If NOISE is non-zero (a positive octal number), normally distributed random noise with standard deviation and mean value specified by input at RAPAR is added to the generated data. The entry at NOISE is used to start the random-number generator.

25	М	RAPAR	05,99	
		 		
. 26	D	01,01	HU ABIAS	
27		04,01	.057	
28	D	01,02	A L H B I A S	
29		04,02	200.	

The RAPAR array is used to indicate bias values for measurements to be generated. Line 25 merely indicates to the program that the array is of maximum size 05,99. Lines 26 and 27 specify that for station HU and the azimuth measurements the bias value to be added is .057 degrees. Lines 28 and 29 indicate that for station AL and the height measurement computed from AL the bias value to be added is 200 feet. For additional entries the same two cards are repeated with increased subscripts.

30		SIGMA	200
31		2	. 1
32		3	.1
33		4	50.
34	I	ISIG	1
35	I	2	2
36	I	3	3
37	I	4	112

Lines 30-37 contain the observation data weighting factors. For each SIGMA entry, a corresponding entry defining the sigma set and data type appears in ISIG Lines 34-37. The ISIG entries are of the form 100I + K, where I is the observation set number and K is the data type. Ten sets, corresponding to I = 0, 1, 2, ..., 9, may be entered. This selected value of I is the same as the entry in Column 5 of the station location card. (See Section 3,4,5.) The data type, K, must be one of those listed in Table 7.

In the above example, range, azimuth and elevation data would contain noise with a sigma of 200 feet, .1 degree and .1 degree respectively, while height would contain noise with a sigma of 5 feet.

1.1		1
20 11 055	D .	1

If elevation is a chosen measurement to be generated, then REFR is the input quantity that allows for elevation refraction correction. The computed elevation, E, is altered to account for refraction, using either

$$E' = E + \eta_{si} \cot E$$

if E ≥ 0.1 radian, or

$$E' = E + \frac{1}{1000} \frac{\eta_{si} \times 10^6}{12 + 1000E} - \frac{80}{6 + 1000E}$$

if E < 0.1 radian and $n_{Si} \neq 0$.

REFR contains the $\eta_{\rm Si}$ term, wherein i = 0, 1, 2, ..., 9. The appropriate value of i is entered on the station card in Column 6 (see Section 3.4.5). Nominally $\eta_{\rm SO}=3.12\times10^{-6}$. Rise, set, and maximum elevation values are determined from the geometric E which represents the elevation before refraction correction is applied. Additional cards may be inserted at this location if necessary.

Table 7.

Data Types for ISIG Entries

Data Type (K)	Data Description	Symbo1
1	Range	R
2	Azimuth	A
3	Elevation	E
4	Topocentric right ascension	αT
5	Topocentric declination	δт
6	Topocentric hour angle	HA
7	Geocentric right ascension	αg
8	Geocentric declination	δg
10	Argument of latitude	u
11	Cross plane	v
12	Height	h
13	ŝ	û
14	ŷ	ŷ
15	ĝ	ĝ
17	Range difference	P
18	Range difference	Q
19	Range rate	Ř
20	R difference	P
21	R difference	ģ

3.4.4 Lines 39-45 Orbit Covariance Matrix

39	ATAS	1.	-4
40	3	.5	-7
41	6	2.	-2
42	10	4	-2
43	15	2000.	
44	21	1.	

If observation uncertainties are to be calculated, a covariance matrix for the ADBARV elements at epoch must be input in lower triangular form at ATAS. The order of the elements is Row 1/Column 1 at ATAS(2), Row 2/Column 2 at ATAS(3).

In addition, the following input is needed.

D 434 OTPOTENTY
RAM I /XXXXXX I
:

The CPRAM variable indicates to the program that the covariance matrix has been input and in the ADBARV notation. (For a more complete explanation of the CPRAM variable see Section 3.3.2).

3.4.5 Station Cards

The locations of tracking stations which are associated with the observations to be generated must be input by means of station cards carrying appropriate descriptive information.

Figure 1 on the next page shows the proper fields for the input that is described below:

- a. Station ID Columns 1 and 2 (ST).
 No two stations may be identified by the same symbol. The three codes that are not permissible as station ID's are TS, TR, TF.
- b. Sigma Index Column 5The sigma index identifies the set of observation sigmas

to be applied to data that is generated from this station (see Section 3.4.3).

- c. Type of Refractivity Correction Column 6

 This indicator selects the type of refractivity correction which is to be applied to elevation readings. (This input depends on previous input. See Section 3.4.3).
- d. Latitude Columns 9-17
 The latitude of the station is entered in degrees.
- e. Longitude Columns 19-27

 The east longitude of the station is entered in degrees also.
- f. Altitude Columns 29-36
 The altitude of the station is entered in feet.
- g. P, Q Indicators Columns 38-39 and 41-42

 If P, Q, P, Q data (i.e., range difference and range rate difference between a master station and two slave stations) is to be generated these columns must contain the station ID's of the slave stations. Also, it is necessary to enter a station card for each slave station but columns 38-39 and 41-42 are to be left blank.

The station cards must be preceded by two cards with END in columns 1-3, and must be followed by a card with TS in columns 1-2.

3.4.6 Data Limit Specification Cards

- a. Station ID (ST) Columns 1-2
- b. Data Rate Columns 9-16

Time interval in seconds at which data for a given station are to be generated and testing interval for rise set option.

c. Minimum Elevation Columns 18-23

The minimum elevation at which the vehicle is visible to this station.

- d. Maximum Elevation Columns 25-30
 The maximum elevation at which the vehicle is visible to this station. Zero value implies a 90 degree limit.
- e. Maximum Range Columns 32-40

 The maximum range in nautical miles to which the vehicle is visible. Zero value causes this test to be ignored.
- f. Start Time Columns 51-58

 Start time from midnight of start date in days, hours, and minutes. Zero value implies that epoch is start time.
- g. Stop Time Columns 60-67

 Stop time from midnight of start date in days, hours, and minutes.

The set of cards must follow the TS card in the deck and themselves be followed by a card with TR in the first two columns.

3.4.7 Data Type Cards

The following set of cards (which are the last in the card deck) specify the exact type of measurements to be generated from each station.

Figure 3 is a card image.

- a. Station ID
- Columns 1-2
- b. Observation Types
- Columns 7-33

 $\,$ An $\,$ X $\,$ in the appropriate column will produce specific measurements according to Table 8.

NOTES	2 K K K K K K K K K K K K K K K K K K K	Station codes must be entered in Columns 38-39 and	41-421f P, Q or P, Q data are input.	An asterisk (*) following a unit value indicates that a decimal point is necessary for that	quantity.													
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			1	1														E
\$7 ST	2												for Card Fornat					
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Altítude pp qq (ft.)* ST ST	23 17 22 24 25 24 25 24 11 12 25 24 25 24 25 27 12 25 24 25 25 25 25 25 25 25 25 25 25 25 25 25																	

	NOTES	ST is the station identification code.	Start and stop times are from midnight of	epoch.	epoch itself is used.	An esterisk (*) fol-	lowing a unit value	decimal point is	necessary for that													
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Start Time	25 12 28 27 28 28 28 28 28 28 28 28 28 28 28 28 28			 - -							-	- - -	 		 		 	+	+	F		+
Maximum Range (n m1)*	32 M M M M M M M M M M M M M M M M M M M															Generation Limits Card Format						
Maximum Elevation (deg.)*	25 25 77 28 25 35 35 35 35 35 35 35 35 35 35 35 35 35															Data Generatio						
Minimum Elevation (deg.)*	18 19 70 21 27 23															Figure 2.						
Interval (sec.)*	9 10 11 12 13 14 15 16																					

Identification	73 74 75 76 77 78 79 80																												
		NOTES	ST is the identifica-	tion code.	If P, P , Q, Q are	fication of an ad-	ditional station-	is necessary.																					
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Table 8.

Output Quantities Corresponding to

Columns 7 through 33 of Data-Generation Type Card

Column	Output Quantity	Unit
7*	Range	n mi (ft on ETAPE)
8*	Azimutḥ	deg
9*	Elevation	deg
10*	Range rate	ft/sec
11-14*	P, Q, P, Q	ft/sec, ft
15	Azimuth rate	deg/min
16	Elevation rate	deg/min
17	Range acceleration	ft/sec ²
18	Mutual visibility (Output will be a list of numbers of stations visible at output time. Stations numbered in order of input on station cards. Number of stations, 8 maximum).	
19	Geodetic latitude of vehicle	deg
20	Longitude of vehicle	deg
21	Surface range from station to subvehicle point	n mi
22*	Altitude of vehicle	n mi (ft on ETAPE)
23	Doppler rate	
24	Look angle (Angle between a vehicle axis and the station/vehicle line of sight. The direction cosines of the vehicle axis in the basic inertial system must be entered in C(37), C(38), and C(39). These quantities	deg

^{*} These quantities are output on ETAPE

Table 8 (cont.)

Column	Output Quantity	Unit
	may be input as constant or the user may provide a subroutine (FANG) to compute the direction cosines at each output point).	
25	Observation uncertainties. (If inverse A^TA matrix for initial conditions is input at ATAS, the ADBARV elements are selected as parameters, and if an X is entered in Column 25, the $[A^TA]^{-1}$ is updated to observation times and the standard deviations in the quantities R, A, E, \dot{R} , \dot{A} , \dot{E} are derived and printed. The uncertainties are only those due to the uncertainty in the ephemeris which is implied by the given $[A^TA]^{-1}$ for the epoch conditions).	Same units as obser- vations
26	Angle kappa (K). (Angle between station line-of-sight and geocentric radius vectors).	deg
27	Aspect angles. (Angle 1 (ϕ) is defined as the angle between the vehicle yaw axis and projection of the station line-of-sight vector in the roll plane. Angle 2 (Θ) is defined as the angle between the vehicle roll axis and the line-of-sight vector to the station.	deg
28	Signal attenuation = $-40 \log_{10}R$, where R is slant range in feet	db
29*	\hat{x} , \hat{y} , \hat{z} (Same rectangular earth-fixed (X through Greenwich) geocentric quantities accepted as Type 5 observations for orbit determination).	n mi (ft on ETAPE)

^{*} These quantities are output on ETAPE

Table 8 (cont.)

Column	Output Quantity	Unit
30*	Topocentric right ascension and declination	deg
31*	Geocentric right ascension and declination	deg
32*	Topocentric hour angle	deg
33*	Vehicle-centered argument of latitude and cross-plan angle	deg

^{*} These quantities are output on ETAPE

3.5 Orbit Determination Data

This section gives a description of all the pertinent data for a differential correction run to be used in conjunction with the previously described basic data.

3.5.1 Lines 1-14 Multiple Satellite Option

As was mentioned in Section 2, TRACE-D will accept measurements for up to six satellites on any one run. The method of specifying the input for these vehicles is shown below.

Year	1	I	SAT2	1964	
Month	2	I	2	2	
Day	3	I	3	10	
Hour	4		4	3.	
Minut	e 5		5	30.	
Secon	d 6		6	52.	
ICTYP	7	I	7	2	
IC	8		8	352.	
2	9		9	10.	
3	10		10	90.05	
4	11		11	165.	
5	12		12	22580632.	
6	13		13	25205.3	
DRAG	14		14	.015	

If observations for a second satellite are to be input, Lines 1 through 14 are used for entry of epoch, initial conditions, and drag coefficient for Satellite 2. Lines 1 through 3 contain the year, month, and day, and Lines 4 through 6 contain the hour, minutes and seconds, Greenwich time. Line 7 indicates the type of initial conditions that may be entered in Lines 8 through 13 (Type 1, 2, 3, 4, 8, or 9). Line 14 contains the drag coefficient (CDA/W). The input initial conditions

(IC) for satellites 3 to 6 are the same as those noted above except that the symbol SAT2 is replaced by SAT3, SAT4, SAT5, and SAT6, as appropriate.

3.5.2 Lines 15-31 Parameter Specification

The method of selecting the parameter set for the differential correction process is described below.

3.5.2.1 <u>Differential Equation Parameters</u>

			-			_	-			 			
15	D	CPRAM	2	x	x	x	x	x	x				
16	D	CPRAM	x										
17	D	3											
18	D	5											
19	D	7											
20	D	9											
21	D	PSAT2											
22	D	PSAT3											
23	D	PSAT4					7						
24	D	PSAT5											
25	D	PSAT6	21										
26	D	KPRAM											
27	D	3		-									

An X entered in any CPRAM, DPRAM, PSAT, or KPRAM character position causes the corresponding parameter to be differentially corrected. The ordering of entries in the CPRAM, DPRAM, PSAT, and KPRAM character position boxes is as follows:

a. <u>CPRAM (Initial Condition Parameters for Satellite 1)</u> (Line 15)

The first position specifies which one of these types of initial conditions is applicable, and succeeding positions indicate the particular parameters that are desired in each case. Ordering of parameter entries for IC Types 1, 2, and 3 is as shown in Section 3.3.2.

b. <u>DPRAM (Differential Equation Parameters)</u> (Lines 16 through 20)

The ordering of DPRAM differential equation parameter entries is as shown in Section 3.3.2. However, in this application the T_1 and T_2 parameters are associated with Satellite 1 only.

c. PSAT2 through PSAT6 (Initial Condition and Drag Coefficient Parameters for Satellites 2-6) (Lines 21 through 25)

The ordering of PSAT IC and drag parameter entries for Satellites 2 through 6 is shown below.

PSAT2	α2	δ2	β2	A ₂	r ₂	v ₂	t ₀₂	DRAG ₂
PSAT3	α3	δ3	β3	A ₃	r3	v ₃	to3	DRAG ₃
PSAT4	αц	δ4	βц	A4	rų	V4	t ₀₄	DRAG ₄
PSAT5	α5	δ ₅	β5	A 5	r ₅	v ₅	to ₅	DRAG ₅
PSAT6	α6	δ ₆	β6	A ₆	r ₆	v ₆	to ₆	DRAG ₆

It is important to note that only IC Type 2 may be specified for Satellites 2 through 6.

d. KPRAM (Orbit Parameters for Satellite 1) (Lines 26 and 27)

Ordering of KPRAM orbit adjust parameters is as previously shown in Section 3.3.2. It should be noted that the orbit adjusts are for Satellite 1 only.

Sixty trajectory parameters is the maximum number which may be selected for simultaneous solution.

3.5.2.2 Radar Parameters

28	М	RAPAR	05, 99	
29	D	01, 01	BNLLAT	
30		03, 01	.01	
31		04, 01		
32	D	01, 02	C K 2 4 R B I A S	
33		03, 02	500.	
34		04, 02	750.	
35	D	01, 03	H U T B I A S	
36		03, 03	.001	
37		04, 03	.0035	

Line 28 indicates that the data listed subsequent to RAPAR on the load sheet will be input into a 5×99 matrix array which has been preset to zero. The columns of this array correspond to parameters, and the rows correspond to parameter identification (Positions 1 and 2), bounds (Position 3), and bias estimates (Position 4) respectively. Row 5 is currently not used.

Lines 29 through 31 specify the first applicable radar parameter. Line 29 contains the station name (Positions 1 and 2), pass identification (Positions 3 and 4), and parameter name (Positions 5 through 10). Lines 30 and 31 contain the bound and initial value, respectively, in feet, degrees, and minutes except for \dot{R} , \dot{P} , and \dot{Q} , which are in feet per second. If the parameter is station latitude, longitude, or altitude, the initial value is taken from the station location card.

If the pass identification character position is left blank, all data with the indicated station name will be used to correct the parameter. If the pass identification is not omitted, only data that are identified by both the indicated station name and indicated pass identification will be used to correct the parameter. If the radar parameter specified is station latitude, longitude, or altitude, the pass identification is ignored and all data with the station name are used for the parameter correction.

Lines 32 through 34 and Lines 35 through 37 specify the second and third radar parameters respectively. Station names, pass identifications, parameter names, bounds, and initial values are treated in the same manner as the inputs in Lines 29 through 31 described above. Additional cards may be added in cases where more than three radar parameters are involved. Available radar parameters are listed in Table 9.

Note that the total number of parameters which may be selected for simultaneous solution must be less than one hundred.

Table 9.

PARAMETER	SYMBOL
Station latitude	LAT
Station longitude	LONG
Station altitude	ALT
Time bias	TBIAS
Range bias	RBIAS
Azimuth bias	ABIAS
Elevation bias	EBIAS
Topocentric right ascension bias	RTBIAS
Topocentric declination bias	DTBIAS
Topocentric hour angle bias	HABIAS
Geocentric right ascension bias	RGBIAS
Geocentric declination bias	DGBIAS
Argument of latitude (u) bias	UBIAS
Cross plane (v) bias	VBIAS
Height bias	HBIAS
$\hat{\mathbf{x}}$ bias	XBIAS
ŷ bias	YBIAS
â bias	ZBIAS
P bias	PBIAS
Q bias	QBIAS
Range-rate bias	RDBIAS
P bias	PDBIAS
Q bias	QDBIAS
Range scale factor (KR)	KR
Range-rate scale factor (KD)	KD

3.5.3 <u>Lines 38-50</u> <u>Parameter Bounds</u>

38	BNDS	.5
39	2	.5
40	3	.1
41	4	.5
42	5	1000.
43	6	5
441	7	.05
45	8	
46	9	
47	10	
48	11	
49	12	
50	13	

A bound must be entered for each parameter selected. These bound entries must be in the same sequence as the parameters. For each iteration of the differential correction process, the change in each parameter is less in absolute value than the corresponding bound if that bound is positive, zero if the corresponding bound is zero, or unrestricted if the corresponding bound is negative.

3.5.4 Lines 51-62 Observation Sigmas

		4	
51		SIGMA	100.
52		2	.5
53		3	.5
54		4	1000.
55		5	200.
56		6	300.
57	I	ISIG	1
58	I	2	2
59	I	3	3
60	I	4	113
61	I	5	114
62	I	6	115

The observation sigmas for each observation type must be input in the same manner as was previously well described in Section 3.4.3.

3.5.5 <u>Line 63 Maximum Iterations</u>

63	I	MAXIT	4

The symbol MAXIT must be input with an integer value to specify a stopping point to the run. If the differential correction process has not converged at the end of MAXIT iterations, the process will be terminated.

3.5.6 Lines 64-66 Residual Editing

64	CEDIT	3	
65	2	.9	
66	3	1	

If CEDIT is zero, no editing is done. If CEDIT is non-zero, residuals will be edited in accordance with the following:

- a. CEDIT < 0 Residuals greater than (input sigma × |CEDIT|) will be discarded.
- b. CEDIT > 0 Residuals greater than (statistical sigma from the previous iteration × CEDIT) will be discarded. No editing is done on Iteration 1. Sigmas are computed for the first five data types encountered for each station.

Line 65 represents a scale factor such that if CEDIT(2) is non-zero, CEDIT is replaced by (CEDIT × CEDIT(2)) at the end of each iteration. If CEDIT(2) is zero, CEDIT is not modified.

Line 66 is a special option wherein if CEDIT(3) is non-zero, Iteration 1 will be repeated with editing performed with the sigmas computed during the first pass through Iteration 1. This will allow editing to be done on all iterations with computed sigmas.

Sigmas (rms) for the first five data types for each station are computed and printed at the end of each iteration regardless of the residual-editing option selected.

3.5.7 Data Correction Factors

3.5.7.1 Lines 67 and 68 Elevation Angle Refraction

67	REFR		
68	2	4.0	-6

A table of refraction indices η_i , which may contain up to ten values, may be input starting at REFR. The entry used to compute refraction corrections for radar elevation observations is determined by the type number contained in Column 6 of the corresponding station location card. A zero in Column 6 causes the entry at REFR to be used, a 1 in Column 6 causes the entry at REFER + 1 to be used, etc.

. If the table contains no entries, the value 312.0×10^{-6} , which is built in at location REFR, will be used to

compute refraction corrections for all data whose station location cards contain zero in Column 6. All other positions of the table are assembled as zeros.

3.5.7.2 Range Refraction Correction

69	RREFC	1	ì

Refraction corrections to all range observations will be computed and applied if RREFC is non-zero.

3.5.7.3 Line 70 Propagation Time Correction

		1	
	2020 1762	i CT TT	70
	1 -2020.1/03	IDLI	70 11
	-2020.1703	SET	/0

The velocity to be used in calculating the observation time correction due to propagation time is entered at SLT in units of earth radii per minute. In the absence of an entry, no correction will be applied. If an entry is present the correction will be applied to times associated with R, A, E, \hat{R} , h, P, Q, \hat{P} and Q data only.

3.5.8 Lines 71, 72 Data Tape Options

71	I	IBCDI	6
72	I	IBINI	1

If the radar observation and station location information is to be input via a BCD tape other than the normal FORTRAN system input tape, the tape number must be specified at IBCDI as 11. If a binary tape containing compacted radar data produced by a previous run is to be input, IBINI must be specified.

3.5.9 Lines 73, 74 True Equinox Correction

73	DALFG	004	
74	2		

An additive factor may be applied to the computed right ascension of Greenwich at midnight of epoch day by entering the appropriate value in units of degrees at DALFG for Vehicle 1, at DAFLG(2) for Vehicle 2, etc. This entry usually is used to correct from mean to true equinox reference coordinates.

3.5.10 Lines 75-78 Proximity Indicator

ф*	75	ANØM1	
λ	76	2	
h	77	3	
R ₀	78	4	

During an orbit determination run, an indicator may be obtained whenever the trajectory passes within a given distance (range) of a point on the surface of the earth by input of geodetic latitude (deg), east longitude (deg), and altitude (n mi) of the point at ANOM1 and the succeeding two positions and of the testing distance (the range from the point to the vehicle) at AMON1(4). Testing and printing is done for up to three such sets of input at AMON1, ANOM2, and ANOM3.

3.5.11 Lines 79 on Parameter Constraint Options

There are two different parameter constraint options available in TRACE-D. Both are described below in detail.

3.5.11.1 General Constraint Matrix

Option 1 allows the user to apply linear constraints to any of the variables in the parameter set, and to specify these constraints by means of an input matrix set up as shown below.

	79	I	KNST 4
	80	I	BLIST 1
	81		1
b ₁₁	82		1
	83	I	2
	84	I	2
b22	85		1
	86	I	3
	87	I	3
b 33	88		1
	89	ī	4
	90	I	4
b44	91		1
	92	I	5
	93	I	1
b ₅₁	94		-1
	95	I	6
	96	I	2
b ₆₂	97		.5
	98		5
	99	I	5
c51	100		6
	101	I	7
	102	I	5
	103		1

The clearest explanation of how this constraint matrix works is an example. Therefore, in the case shown above it is assumed that n parameters are to be solved for where $(p_1,\ p_2,\ \dots,\ p^n) \ = \ P.$ The ordering of the P_1 corresponds to the

order of the X's for the CPRAM, DPRAM, and KPRAM and the RAPAR arrays, respectively. Further assuming that these parameters are to be subjected to m linear constraints, which, for example for n=6 and m=2 might be $p_1+p_5=6$, $p_2-2p_6=0$, KNST above would be equal to (n-m)=4, or the number of effective (unconstrained) parameters.

The BLIST constraint matrix is represented by the factor B in the expression $p = B\bar{p} + c$, where the \bar{p} are the effective parameters. In connection with the foregoing example, this expression would assume the form

$$\begin{bmatrix}
p_1 \\
p_2 \\
p_3 \\
p_4 \\
p_5 \\
p_6
\end{bmatrix} = \begin{bmatrix}
1 & 0 & 0 & 0 \\
0 & 1 & 0 & 0 \\
0 & 0 & 1 & 0 \\
0 & 0 & 0 & 1 \\
-1 & 0 & 0 & 0 \\
0 & .5 & 0 & 0
\end{bmatrix} \times \begin{bmatrix}
\bar{p}_1 \\
\bar{p}_2 \\
\bar{p}_3 \\
\bar{p}_4
\end{bmatrix} + \begin{bmatrix}
0 \\
0 \\
0 \\
6 \\
0
\end{bmatrix}$$

Pertinent constraints are applied by input of the augmented (n + 1) by (n - m + 1) matrix

$$\begin{bmatrix} B & c \\ 0 & 1 \end{bmatrix}$$

in the BLIST array. If a_{ij} is an element of this augmented matrix, then i, j, and a_{ij} would be input. The inputs for the example given above would be as indicated in Lines 79-103. KNST (line 70) is input as 4 and then the BLIST matrix follows. Lines 80, 81, and 82 specify that BLIST (1, 1) is a 1 and lines 83, 84, and 85 that BLIST (2, 2) is a 1, etc. Elements of the matrix not input are assumed to be zero. In this way any subset of the set of parameters may be linearly constrained and the constraint matrix may be input to the program in the exact same manner.

3.5.11.2 Special Application to Station Location

The other option available is a specific case of the general constraint matrix which is applicable in the following type of problem. Consider a differential correction run with data from a tristatic system and a set of parameters including the latitudes, longitudes and altitudes of the three stations. In such a case, by choosing this constraint option, the correction of the station coordinates can be performed such that the baseline distances are held constant.

Mathematically, this implies that three constraining equations are applied to the nine station locations; more specifically they are of the following form.

$$(\theta_1, \phi_1, H_1)$$
 are the three sets of latitude,
 (θ_2, ϕ_2, H_2) Longitude, and altitude for
Stations 1, 2, and 3.
 (θ_3, ϕ_3, H_3)

and a_i , b_i , c_i i = 1, ..., 6 are the 18 coefficients of the three equations.

With the equations in this particular form, it seems that the general constraint option could be applied easily. However, there are two reasons for the separate treatment of this application that are not immediately apparent. First, the constants a_i , b_i , c_i $i=1,\ldots,6$ are functions of the current station location² and are not easily and accurately calculable by the user. Second, since

The detailed derivation of this particular form of the constraining equations is not given here but may be found in Reference 3.

The exact expressions for the coefficients can be found in Reference 3.

the constants <u>are</u> functions of the current station locations, they must be reevaluated every time the station locations change (i.e., after every iteration of the correction process the constants must be reset since the station locations have been adjusted). In other words, the type of constraint matrix needed here is a dynamic one that is adaptable to change throughout the estimation procedure. It is now obvious that the general constraint matrix of Section 3.5.11.1 is too rigid for this purpose.

Thus, added to the TRACE-D program is the capability to compute these necessary constants from input information, insert them into the appropriate location of the constraint matrix, recompute the constants as a function of the new station locations after each iteration and adjust the constraint matrix accordingly. Once the user has set up the appropriate input the rest is performed by the program.

The input necessary is best described with an example. Consider a differential correction run with data from three stations and a parameter set consisting of the ADBARV elements, drag, and station locations. To employ the fixed baseline distance constraints on the station locations consider B in the following expression.

$$\Delta \rho' = B \Delta P + c$$

There are 16 parameters to be estimated but there are 3 constraint equations, therefore there are 13 effective or unconstrainted parameters. B is then of dimension 16×13 and looks like this:

[Δρ']	= [B]	[Δρ]	[c]
Δα	10000000000000	Δα	0
δΔ	01000000 0 0 0 0 0	δΔ	0
ΔB	00100000000000	ΔB	0
ΔA	00010000000000	ΔΑ	0
ΔR	00001000000000	ΔR	0
ΔV	000001000000000	ΔV	0
△ drag	00000010000000	∆ drag	0
Δ lat _l =	0 0 0 0 0 0 0 a ₁ a ₂ a ₃ a ₄ a ₅ a ₆	∆ long ₁ +	0
△ long ₁	0000000100000	∆ alt _l	0
△ alt ₁	0000000010000	∆ long ₂	0
△ lat ₂	0 0 0 0 0 0 0 b ₁ b ₂ b ₃ b ₄ b ₅ b ₆	∆ alt ₂	0
△ long ₂	00000000001000	∆ lat ₃	0
△ alt ₂	00000000000100	∆ alt ₃	0
△ lat ₃	000000000000000000000000000000000000000	-	0
△ long ₃	0 0 0 0 0 0 0 c ₁ c ₂ c ₃ c ₄ c ₅ c ₆		0
△ alt ₃	0 0 0 0 0 0 0 0 0 0 0 0 0 1		0

The quantities a_i , b_i , c_i , i = 1, ..., 6 are, of course, the coefficients in the constraint equations which are unknown to the user.

This B matrix is input in exactly the same manner as the general constraint matrix except that each element that is a coefficient (either a_i , b_i , c_i) must be input with a value of - 10,000. This is merely to indicate to the program the position in the matrix of these terms.

Lines 104 on show the appropriate format for the necessary input of this case.

104		NUMB		116	I	8
105	I	44	-1	117	I	8
106	Ī	KNST	13	118	I	-10,000.
107	I	BLIST	1	119	I	8
108	I		1	120	I	9
109			1	121		-10,000.
110	I		2			
111	I		2		etc.	1
112			1			
113						
114	etc.					
115						

Lines 1.04 and 105 specify the quantity NUMB(44) which must be input as a - 1 to choose this constraint option. Line 106 is the number of unconstrained parameters in the parameter set. Lines 107 on are the non-zero elements of the B matrix entered in order.

3.5.12 Station Identification Cards

The locations of tracking stations or of points on the surface of the earth which are associated with observations must be input by means of station cards carrying appropriate information indicating the manner in which the corresponding observations are to be processed. These cards were previously discussed in Section 3.4.5 and shown in Figure 1, but the format is included again here for completeness.

- a. Columns 1 and 2 (ST): Station identification symbol.

 No two stations may be identified by the same symbol or any one station by the symbol TS.
- b. <u>Column 5:</u> Sigma index identifying observation-sigma set to be applied to data from corresponding station. The sets of sigmas are input with the base data.
- c. Column 6: Type of refractivity correction to be used for elevation readings from this station. Refractivities are numbered in their input order within the base data (see Line 67, REFR).

- d. Columns 9 through 17: North latitude of station in degrees.
- e. <u>Columns 19 through 27</u>: East longitude of station in degrees.
- f. Columns 29 through 36: Altitude of station in feet.
- g. Columns 38/39 and 41/42: If a station reports P, Q, or P, Q data, Columns 38/39 and 41/42 contain the two letter symbols for the associated station(s) of the tracking configuration. Each such associated station must be represented by a separate station card, but it is not necessary for Columns 38/39 and 41/42 to be filled out on the latter.

These cards must be preceded by a card with END in Columns 1-3 and followed by a card with TS in Columns 1 and 2.

3.5.13 Observation Data Cards

The observations to be processed must be the last set of cards in the deck and must follow the station location cards.

Since the number of observations that may be input to TRACE-D is unlimited, there is a flocking procedure that must be followed. A flock of data consists of 200 or less observation cards for a single satellite. There is no limit to the number of flocks that can be stacked; however, each flock must be followed by a card with TF in Columns 1 and 2 and the times associated with the observations of a flock can never be earlier than the latest time of the previous flock. This means that the data is not time sorted within a flock but the flocks are sorted according to earliest and latest times therein contained.

The contents of an observation card is formatted in the following way, as shown in Figure 4.

- a. Columns 1 and 2 (ST): Station Identification, symbol which must correspond to a station location card.
- b. Columns 3 and 4: Pass identification (optional).
- c. Columns 5 through 21: month (columns 5 and 6), day (columns 7 and 8), hours (columns 9 and 10)

minutes (columns 11 and 12), and seconds (columns 13-21), of the corresponding observations relative to Greenwich Mean Time.

- d. Column 22: Observation set number.
- e. Columns 23-76: Observation 1 (columns 23-40), Observation 2 (columns 41-58), Observation 3 (columns 59-76).
- f. Column 77: Card number indicating observations, variances, or covariances.

The observation set (d) number and the card number (f) are the two indicators that define exactly what type of observations are contained on each card. Table 10 gives a complete listing of all types according to observation set number and card number.

After the last observation card in the deck, a TF card is not necessary, however a card with TR in Columns 1 and 2 plus an END card must be attached as the last two cards of the deck. If data from more than one satellite are to be used, the Satellite 1 data are set up in the same manner except that the TR card must be replaced by a TT card. The data for Satellite 2 are then similarly arranged. If Satellite 2 is the last vehicle, corresponding data are followed by a TR card and an END card: if it is not the last satellite, data are followed by a TT card. Data for Satellites 3 through 6, as applicable, are added in the same manner. A TR card rather than a TT card must follow the data corresponding to the last satellite, and an END card must follow the TR card. See Section 3.6 for a picture of the correct setup.

3.6 Input Deck Arrangements

Since the basic running deck to be used for each function to be performed can be obtained, the user need not concern himself with its contents. Therefore in each of the Figures the separate parts of this deck are ignored and it is labeled totally as the basic running deck. The categories of data used are described in detail in previous sections (for instance, Basic Data is explained in Section 3.2, etc.).

Field 3	Elevation(E) Variance(E) Covariance(A, E)	Topocentric hour angle (HA) Variance(HA) Covariance(&T,HA)		Altitude(h) Variance(h) Covariance(v,h)	\hat{z} Variance(\hat{z}) Covariance(\hat{y},\hat{z})	Range difference(Q) Variance(Q) Covariance(P,Q)	Range rate differences(Q) Variance(Q) Covariance(P,Q)
Field 2	Azimuth (A) Variance(A) Covariance(R,E)	Topocentric declination($\delta_{ extbf{T}}$) Variance($\delta_{ extbf{T}}$)	Geocentric declination(δ_{g}) Variance(δ_{g})	Cross plane(v) Variance(v) Covariance(u,r)	\hat{y} Variance (\hat{y}) Covariance (\hat{x},\hat{z})	Range difference(P) Variance(P) Covariance(R,Q)	Range rate difference(è) Variance(è) Covariance(k, è)
Field 1	Slant range(R) Variance(R) Covariance(R,A)	Topocentric right ascension (α_T) Variance (α_T) Covariance (α_T, δ_T)	Geocentric right ascension(α_g) Variance(α_g) Covariance(α_g , δ_g)	Argument of latitude(u) Variance(u) Covariance(u,v)	$\hat{\mathbf{x}}$ Variance($\hat{\mathbf{x}}$) Covariance($\hat{\mathbf{x}}$, $\hat{\mathbf{y}}$)	Slant range(R) Variance(R) Covariance(R,P)	Range rate(Ř) Variance(Ř) Covariance(Ř, P)
Observation Card Type (Column 77)	0 1 2	0 1 2	0 1 2	0 1 2	0 1 2	0 1 2	0 1 2
Observation Set Number (Column 22)	1 1 1	2 2 2	ო ოო	7 7 7	יטיטיט	9	7 7

Table 10. Observation Types and Indicators

3.6.1 Trajectory Prediction Deck Arrangement

When the function to be performed is a single trajectory prediction (function code ITIN = 3), the arrangement is as in Figure 5.

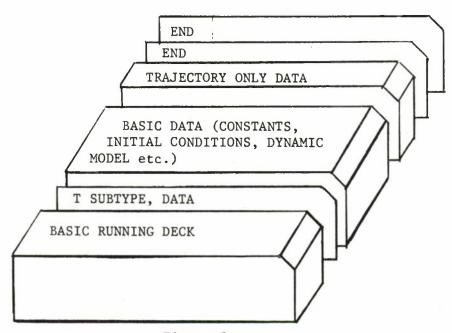


Figure 5.

TRAJECTORY PREDICTION DECK ARRANGEMENT

When several trajectory predictions are to be done in one run (function code ITIN = 333, etc.) then the deck arrangement is merely an extension of that for the single case (Figure 6).

3.6.2 Observation Generation Deck Arrangement

Figure 7 and Figure 8 show the correct data setup for a single data generation run (function code ITIN = 4) and several cases (function code ITIN = 4.4, etc.) respectively.

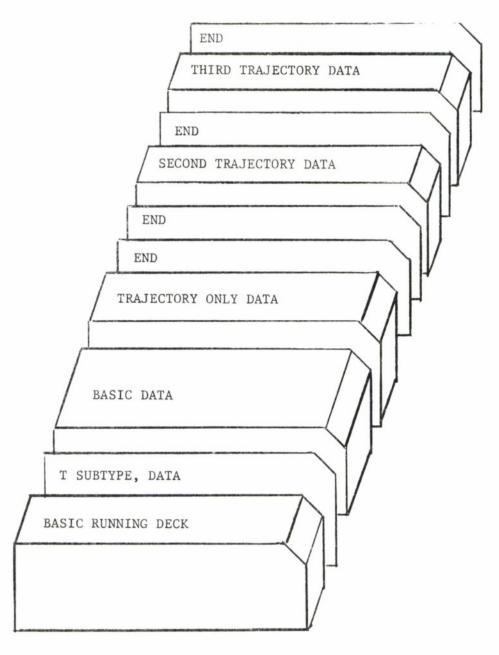
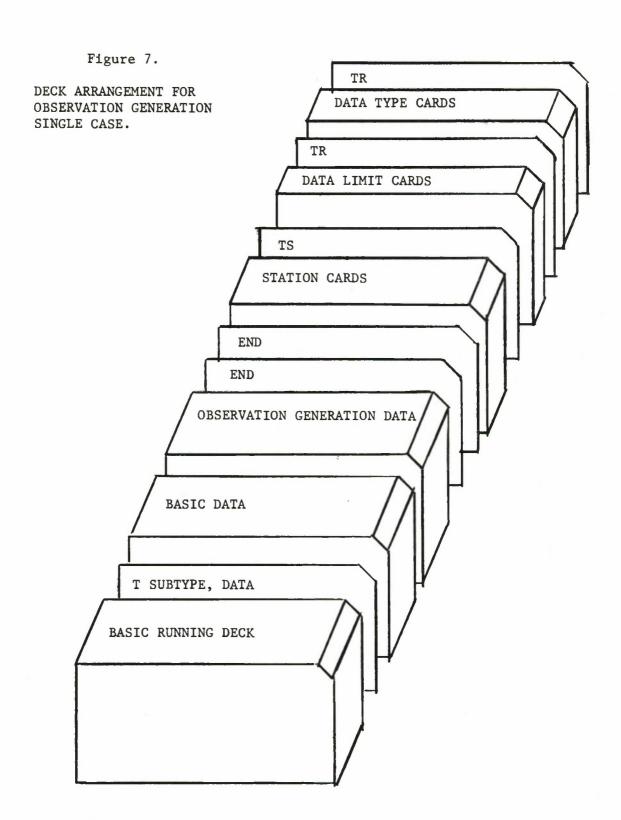
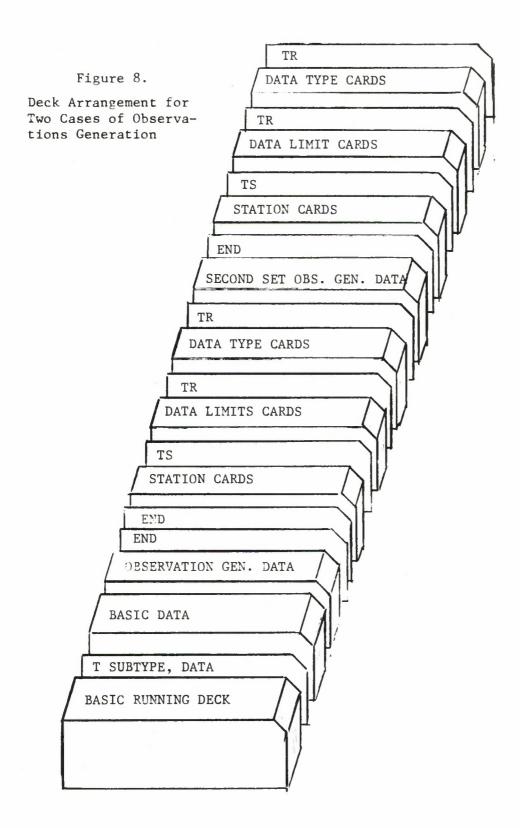


Figure 6.

MULTIPLE TRAJECTORY PREDICTIONS DECK ARRANGEMENT





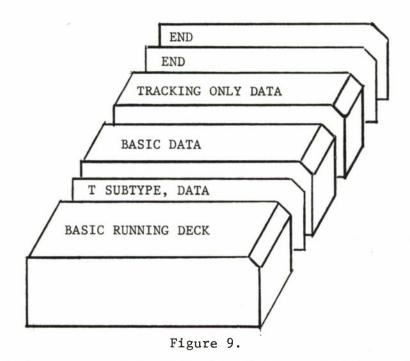
3.6.3 Orbit Determination Deck Arrangement

There are several different deck setups that are permissible for an orbit determination run (function code ITIN = 12) according to the choice of several suboptions.

Figure 9 is the simplest deck setup and applies when the observation data is being input on tape (i.e., IBCDI input variable is used).

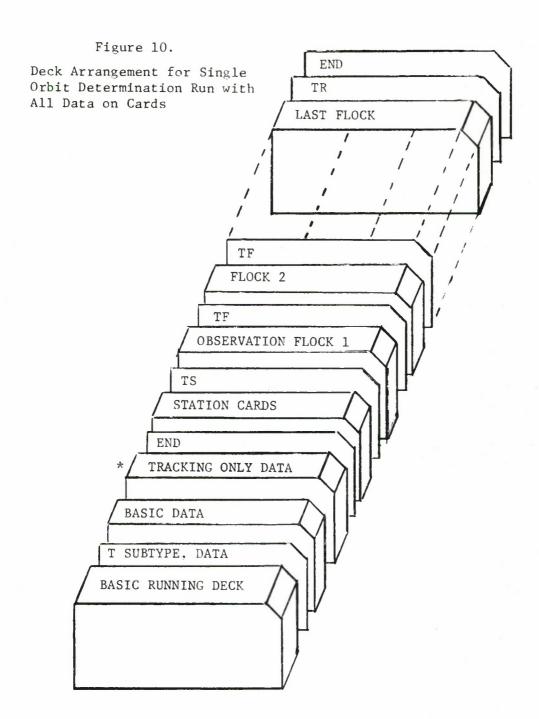
Figure 10 is the ordinary deck setup for a single case when the observation data is attached to the deck. Figure 11 is the deck setup for two such stacked cases.

Figure 12 is the appropriate data arrangement for the situation of multiple satellites (in this case three satellites).

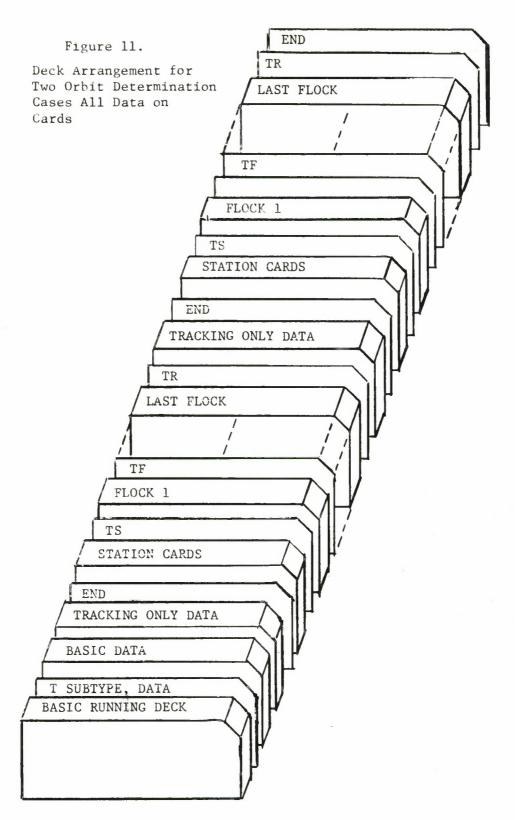


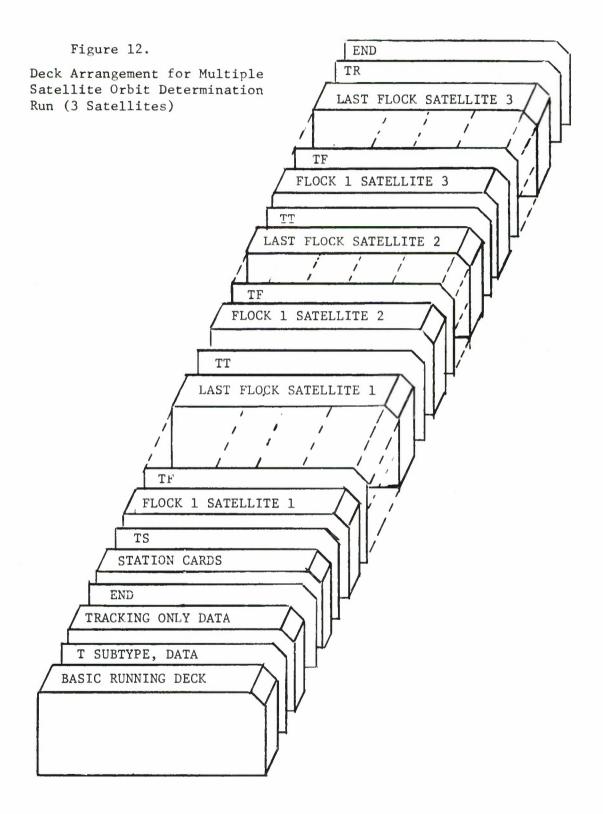
Deck Arrangement for Orbit Determination with Input Tape*

* Note that the BCD tape of observations must contain as its first set of cards the station cards followed by a TS card and then the observations in proper flocks followed by TF cards with a TR card replacing the TF card of the last flock.



^{*} Note that the word "tracking" is used interchangeably with the words "Orbit Determination".





3.6.4 Sample Input Decks

Figures 13, 14, and 15 are listings of sample data decks for trajectory prediction, observation generation, and orbit determination. Besides giving the user an idea of what a typical deck looks like, they may also be used to familiarize the user with the operation of TRACE-D before he creates his own input. Another reason for running a test case of this sort is to determine the status of the program tape, for it is possible for the contents of a tape to deterioriate and no longer be useful¹.

It is not to be assumed that these sample cases exercise all the possible options of TRACE-D, but rather that they exhibit typical input and output. A complete description of the output obtained from these runs is included in Section 4.

In this instance, there is no cause for alarm. MITRE has the capability to create a new and correct program tape in 24 hours.

Figure 13.

																																						1					
							-7						1											a second					9		Q I	B -	D	-8	0.1	00	හ •	71	<u>π</u>	61			
							-	• 0					community and the community an									15							-•114		.2390598	498699	.2122685	.1291007	.1839230	.3299649	3	0	. 440156	4173952			
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Σ	7	316.7706	-17007,799540638
Σ	7	145321.21852	953.51541
Σ	7	145325.56644	-16893.817585227
M	1	45329,96037	16841.8645012
Ψ	7	145334 • 44229	16781 • 98687660
Σ	7	145338,72621	3.0262466
Σ	7	145342,55615	568.61660103
ΙΣ,	7	145343.53946	.75189147
Ψ	7	145346,43408	2.44652223
Ξ	7	145350,28802	-16554.962598321
Σ	7	145354.04795	16497.40190
Σ	7	145357,94188	-16436•200131176
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Σ	7	145416.79557	16115.79396319
Ξ	7	145420,59551	16046.08792644
Σ	7	145422 • 45482	9391437
Σ	_	45424 • 35545	5975.29658788
Ξ	7	145428,11539	905.686
Σ	7	4543	-15828.20209968
Σ	7	145434 • 11063	73186.28604058
MI	_	145435,63527	15751.77450622
IΨ	7	145439,39521	367452
Σ	7	145443,15515	-15592.9317584
IΣ	7	145445.57845	579.59313911
Σ	7	45446.9150	-15510 3976377
Σ	7	145450 • 6750	-15425.73326766
MH	7	145454 43497	-15338.88615482
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Σ	7	1455 1.95486	-15158.382217763
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Σ	8145535.794350	-14222-11318	
MH	8145539 554296	-14104.28313642	
Σ	145542 353595	6651813 • /466 /2 /0	
ΣIΣ	8145547.074189	-13859.5675852	
Ψ	45550 B34137	-13732.53379261	
ΙΣ	8145553.633436	6495847.08001626	
MH	8145554.594085	-13602.29002612	
Ξ	8145558,354036	-13468,76377951	
MH	81456 2.113986	-13331.38549864	
Ξ	81456 4.913282	6344314.04196078	
Ξ	81456 5.873934	-13191.59317582	
Ξ	81456 9.633882	-13047.79954063	
Ξ	8145613,393830	-12900.44488185	
Ξ	8145616 193133	6197545-17712308	
Ξ	8145617,153781	-12749.44717848	
Σ	8145620,913730	-12594.75885820	
MH	8145624,673682	-12436.28740155	
Ι	8145627.472989	6055927.46057070	
Σ	8145628,433635	-12273,99343830	
Ξ	8145631.817593	-12124.56955379	
Σ	8145656.800643	5714590.38711481	
IΣ	8145657,479294	-10883.78543305	
ВН	8145657.479294	-11177-12893694	
Ξ	81457 1.239252	-10685,35695534	
ВН	81457 1.239252	-10985.44061678	
ΙΣ	457 4.999211	-10482.5357611	
BH	81457 4,999211	-10789.37040680	
Ξ	81457 8,759171	-10275.27165353	
ВО	81457 8.759171	-10406.45866137	
ВН	81457 8.759171	-10588-92585301	
Ξ	8145711.088489	5564041 • 17449886	er e
Ξ	8145712,519133	-10063.54068237	
ВН	8145712,519133	-10384.057414	1
ΙΣ	8145716.279097	-9847,31233596	
90	8145716.279097	-9987.44849079	
ВН	8145716.279097	-10174.79363512	
Ι	8145720.039062	-9626.57053804	
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Σ	8145722•36837	3289 • 17318641	
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g u	8145723 79903	9742.77821	
ΣH	8145727,08899	9200.43700784	
90	8145727.08899	4.0331364	
ВН	8145727.08899	9548.05216532	
Σ	8145731,31895	37.069553	
30	8145731,31895	08759838	
ΒH	8145731.31895	•64074802	
Ξ	8145733,64827	31494082	
Σ	8145735.07892	1302493	
90	8145735.07892	91141730	
BH H	8145735.07892	71981626	
IΣ	8145738 • 83888	6591207	
80	8145738,83888	5538055	
ВН	8145738 83888	28740155	
Σ	8145742.59885	06.6745406	
BD	8145742.59865	•48097109	
BH	8145742.59885	83,32480311	
Ξ	8145744,92817	5255145.669280096	
Σ	8145746.35882	54.19	
90	8145746,35882	81	
BH	8145746,35882	37.75	
IΣ	8145749.46080	63513	
œ H	8145749.46080	31.8033989	
Σ	8145753,87876	435.91141730	
9H	8145753.87876	-7833,28969815	
Ξ	8145756.20808	4.52752641	
IΣ	8145757.63873	170.20702093	
æ H	8145757,63873	574.38615486	
Ξ	81458 1.39870	900.2224409	
ВН	81458 1.39870	.07644355	
Ξ	81458 5.15868	-6626.022637784	
ВН	81458 5.15868	-7043.49179786	
Ξ	81458 7.48800	5091246.948790910	
IΣ	81458 8.91865	-6347.6998031	
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BH	81459 1.55	843	-2583.83366142	
Σ	81459 5.78	842	-1728,55249343	
ВО	81459 5.78	845	-2006 • 36056429	
ВН	81459 5.78		-2223.667	
M	81459 8.39	975	4845091 • 108886	
CB	81459 8.39	975	4882650 • 95141557	
ВН	81459 8.39	975	4857161 • 15484592	
Σ	81459 9.54	841	-1404.35039369	
BD	81459 9.54	941	-1685.668963	
ВН	81459 9.54	841	-1901 • 72309710	
Σ	8145913,30	841	-1079.07	
90	8145913,30	341	-1363.63	
ВН	8145913,30	841	-1578.37	
Σ	8145917.06	840	-752.93	
90	814591	84087	-1040.58	
BH	814591	84087	-1253.7919947	
Σ	814592	84087	-426.21587926	
BD	814592	84087	-716.666994	
ВН	81	84087	-928.16633858	
Ξ	814592	57471	4832679•461913	
BD	814592	57471	4866340.15	
ВН	8145921.93	574	4837948.622008	
Σ	8145924.58	m	-99-17158792	
BD	8145924.58	841	-392,19127296	
BH	8145924.58	941	-601.8362860	
Z I	8145928.37	840	230.58103674	
BD	8145928.37	840	-64.97801837	
ВН	8145928.37	84097	-272.51148293	
Σ	8145932.1	0	557.538713	
CA	8145932.1	840	259.74409448	
BH	8145932.13	84077	54.458989501	
¥	8145934.71	97491	4835563.8779	
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BH	814	64:	4843354.790006049	
IΨ	4	948.048432	933,40387138	
BD	814	948.0	.10531494	
HE	814	5948.048432	434.74999999	
Ι	814	5951,808435	255.42027556	
BD	814	5951.80	950 1 68963	
ВН	814	5951 • 808435	758.81922571	
Σ	814	5955.568442	575.7	
BD	814	5955.56	269.76049867	
BH	814	5955	81.48884512	
Σ	81		194.192870	
BD	81	957.655790	50.42648263	
E	8		29.0353999	
IΣ	8	328452	94.118110	
BD	8		2587.678149581	
BH	8		12.61482937	
Σ	81		10.3517060	
80	8		812333	
BH	81		21.91	
Ξ	81	848480	24.23458004	
BD	81	84848	17.5695537	
BH	81		39.201443	
Σ	81	93582	912595.63644362	
BD	81	93582	932098.6876523	
BH	81		4894511.450103209	
Ξ	81	608	5.54494747	
90	81	010.6084957	3529.190288693	
ВН	8	608	354.29265089	
Ξ	8 1	368	144.	
BD	81	368	838.2014435	
ВН	8	014.3685077	901902	
Ξ	81	.128	4449.713910728	
BD	7 815	018,1285227	4144.511154830	
BH	81	18.12852	3976.858923867	
Σ	8	20.21587	95952	
30	8	20.21587	975564 66534	
BH	8	20.2158	36068.04458579	
Ι	81	21.88853	4752.19127294	
30	00	21.88853	47.9288057	
II	8	21,8885	283.96555113	
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85587 85587 855807 19351 1	748.2611546 588.0593831 347.1167978 347.1167978 3488.9333989 346.9159845 255.1837151 990.33.0085301 186.4350393 933.0085301 634.4711285 634.4711285 921.4238581 845.6692499 728.1823725	
7 815 025 6485587 7 815 029 4085807 7 815 029 4085807 7 815 029 4085807 7 815 021 8719351 7 815 031 8719351 7 815 031 8719351 7 815 031 8719351 7 815 033 1686047 7 815 033 1686047 7 815 033 1686047 7 815 034 9986227 7 815 040 7586437 7 815 040 7586437 7 815 040 7586437 7 815 040 7586437 7 815 040 7586437 7 815 040 7586437 7 815 040 7586707 7 815 048 7186957 7 815 048 7186957 7 815 052 4787237 7 815 055 5600901 7 815 055 5600901 7 815 055 5600901 7 815 055 5600901 7 815 055 5600901	588 • 059383 347 • 116797 346 • 913984 255 • 183715 255 • 183715 338 • 932086 338 • 932086 338 • 93218 345 • 471128 485 • 930118 921 • 423858 345 • 669249 776 • 171915 776 • 171915 530 • 578740	
7 815 029 4085807 7 815 029 4085807 7 815 021 8719351 7 815 031 8719351 7 815 031 8719351 7 815 031 8719351 7 815 033 1686047 7 815 033 1686047 7 815 033 1686047 7 815 033 1686047 7 815 034 9986227 7 815 040 7586437 7 815 040 7586437 7 815 040 7586437 7 815 040 7586437 7 815 040 7586437 7 815 040 7586707 7 815 048 7186957 7 815 048 7186957 7 815 048 7186957 7 815 052 4787237 7 815 052 4787237 7 815 055 5600901 7 815 055 5600901 7 815 055 5600901 7 815 055 5600901 7 815 055 5600901	347.116797 345.252952 388.933398 346.915984 255.18375 539.257545 338.932086 338.932086 338.932086 338.93208 338.93208 338.9320 338.932	
7 815 029 4085807 7 815 021 8719351 7 815 031 8719351 7 815 031 8719351 7 815 031 8719351 7 815 033 1686047 7 815 033 1686047 7 815 033 1686047 7 815 033 1686047 7 815 034 9986227 7 815 040 7586437 7 815 040 7586437 7 815 040 7586437 7 815 040 7586437 7 815 040 7586437 7 815 040 7586437 7 815 048 7186957 7 815 048 7186957 7 815 052 4787237 7 815 055 5600901 7 815 055 5600901 7 815 055 5600901 7 815 055 5600901 7 815 055 5600901 7 815 055 5600901	2525252 3889933398 3466915984 255.183715 900.393675 539.257545 539.257545 338.932086 338.932086 934.471128 921.423858 921.423858 921.423858 921.423858	
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7 815 040 7586437 7 815 043 9040091 7 815 043 9040091 7 815 044 9586707 7 815 044 9586707 7 815 048 7186957 7 815 048 7186957 7 815 048 7186957 7 815 052 4787237 7 815 052 4787237 7 815 052 4787237 7 815 055 5600901 7 815 055 5600901 7 815 055 5600901 7 815 055 5600901 7 815 055 5600901 7 815 055 5600901	5776-17191597 5921-42385810 5945-66924998 5728-18237258 5530-57874012 5236-34711280	
7 815 043 9040091 7 815 043 9040091 7 815 044 9586707 7 815 044 9586707 7 815 044 9586707 7 815 048 7186957 7 815 048 7186957 7 815 052 4787237 7 815 055 5600901 7 815 055 5600901 7 815 055 5600901 7 815 055 5600901 7 815 055 5600901 7 815 055 5600901	0921.42385810 9845.66924998 5728.18237258 5530.57874012 5236.34711280	
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7 815 048 7186957 7 815 048 7186957 7 815 052 4787237 7 815 052 4787237 7 815 055 5600901 7 815 055 5600901 7 815 055 2387537 7 815 056 2387537	806.551181	
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7 815 052-4787237 7 815 052-4787237 7 815 052-4787237 7 815 055-5600901 7 815 055-5600901 7 815 056-2387537 7 815 056-2387537	378,1082676	
7 815 052 4787237 7 815 052 4787237 7 815 055 5600901 7 815 055 5600901 7 815 055 2387537 7 815 056 2387537	078.33694219	
7 815 055 4787237 7 815 055 5600901 7 815 055 5600901 7 815 055 2387537 7 815 056 2387537	6788.751968443	
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7 815 055,5600901 7 815 055,5600901 7 815 056,2387537 7 815 056,2387537	1103.7729486	
7 815 055.5600901 7 815 056.2387537 7 815 056.2387537	76625.852996039	
7 815 056.2387537 7 815 056.2387537	131899.540648845	
7 815 056,23875	7345.880905449	
	7058.797900200	
7 815 056,23875	6930.158792585	
7 815 059,99878	609.087	
7 815 059,99	7324.712926447	
815 059,998787		
7 815 1 3.75881	867.92519	
7 815 1 3.75881	14695	
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figure I) (c	5214070•603636997 8122•322834610	8	7726.558726966		8096-620406776	2985563	61286079	.9878608	8237.50295269	6860.45734	8591.19717	8485.35039	5366496.7191156	5365318 11019	5317782,283416	9098,269356	8832.20800	8730 • 143	9330 • 004921	9067,30971121	8968-818	9559.574474990	9300.414	9205.468	0550833	20865	5442693.471099318	18208652	.52821	5.01246	304453	3.61515	665.61187	219.11023610	0.64829391	9885.977690219	09317	10183-123359500	4 1	F86.08920236	RE7.08687734	63.18893401	532-6400917	
	7 815 1 6.8401781 7 815 1 7.5188437	815 1 7.51884	815 1 7,518843	815 111.278874	815 111.2	5 111	815 115.068	815 115,068	815 1	815 1	815 1	815 1	815 1	815 1	815 1	815 1	815 1	815 1	815 1	815	815 1	815 1	815 1	815 1	815 133,53642	815 133,536421	815 133,536421	815 133,93309	815 133,933090	815 133,93309	815 137,787126	815 137,78712	815 137,78712	815 141 • 54716	815 141.547163	815 141.547163	815 145,307202	815 145,30720	815 145 307202	815 146 320552	B16 146.320652	815, 146, 32055	814 140-06794V	217.00
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BD	8	152.82728	10595.08858257	
BH	81	152.82728	10520,08136474	
Σ	8	156.61732	11030.09153532	
BD	81	156.6173	10796-12467181	
ВН	81	156.61732	10724.21292644	
Σ	81	157,98618	5751823.62200862	
BD	81	157,98618	5741009•71127236	
ВН	81	157.	5690133.1364	
Ξ	81	2 ,37737	11221.51246708	
BD	8	2 ,37737	10991 • 20997363	
BH	81	2 .37737	10922.2847768	
IΨ	81	2 4.20142	11411.81758516	
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ВН	81	2 4.20142	11119.24606293	
Ξ	81	2 8.36746	11614 • 18536734	
9D	81	2 8,36746	11391.668	
ВН	81	2 8,36746	11328,86023610	
Ξ	81	2 9.82081	5886674.21255422	
BD	81	2 9.82081	5873193.56951837	
ВН	81	2 9.82081	5821524.179747	
IΣ	8	212,12751	11792.44488179	
BD	81	212.1275	11573,56627285	
ВН	81	212,12751	11513.57152217	
Σ	81	215,88755	11966.6332020	
BD	81	215,88755	11751 • 36515742	
ВН	81	215,88755	11694.01706027	
MH	8 1	220.02360	12153,58366	
BD	81	220.02360	11942.33136475	
B	81	220.02360	11887.83628600	
Σ	8	221 • 29979	6023854 • 39630069	
BD	81	221.29979	6007901.54196090	
ВН	8	221.29979	5955575.68893397	
Σ	8	223,78365	12319.37303143	
90	81	223,78365	12111.74048548	
Œ	8	223,78365	12059.77985554	
Σ	81	227.54369	12481 • 275262	
RD	8	227,54369	12277-15616792	
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Figure 15 (cont.)

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Figure 15	51.15059041	5810366	81.69258516	348.26148283	92.63517	.040682	42486	41108	95636469	13619.2106298	9499-90151896	7476728	1265.74801580	20669	0669281	444554	2657467	42158788	10564291	99311017	0091848	.33070856	3148.65481508	1.84377943	7728.37924	5.50754582	•43536734	.39304453	19.1223752	2.00492113	240.51476365	529,9025589	375.76902878	.72	0747.34249824	6882935.334624562	83.89102084	14637,905839799	14486.576771555	14468.010498583	14743.215879141	68497	77.505944
	815 252 19602	815 252 196026	815 755 74406 815 755 74406	815 255.244066	815 259,004117	15 259,00411	815 259,004117	815 3 2.7641	815 3 2.764168	815 3 2.764168	815 3 4.5295311	815 3 4.5295311	815 3 4.5295311	815 3 6,524221	815 3 6.524221	815 3 6.52422	815 310 284273	815 310,28427	815 310,284273	815 314,044327	815 314 04432	815 314.044327	815 315,8096931	815 315,8096931	815 315,8096931	815 317 804382	815 317,804382	815 317,804382	815 321,56443	815 321.564437	815 321,564437	815 325 32449	815 325,32449	815 325,324	815 327.0898581	815 327,0898581	815 327 0898581	815 329,08454	815 329,084	815 329 08454	815 332,84460	815 332,844	815 332.84460
	ī	BD	I C	BH	Σ	OB BD	EH	IΣ	BD	E E	Ξ	BD	Œ	I	90	ВН	Ψ	ВВ	B	¥.	98		Ξ.	90	BO	IΣ	BD	ВН	I E	GB	HB	Σ	OH	ВН	Ξ	08	BH	I V	GB	HC	N	GB	ī

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Section 4.

SAMPLE OUTPUT

4.0 This section presents the actual output from the test cases described in Section 3.6.4 whose input is listed in Figures 13, 14, and 15. Each test case is covered separately and the code numbers next to certain sections of the output correspond to the numbered paragraphs of the explanation that follows.

Due to lack of space only pieces of the total output are shown; however, the full actual output is available.

4.1 Trajectory Prediction Output

The following sequenced paragraphs describe the different parts of trajectory prediction test case output shown in Figures 16 to 19.

- The constants used in the program (c, INTEG, NUMB, IFLAG) are printed out here in exact input card image.
- 2. These numbers are the geopotential inputs printed out exactly as read in.
- 3. The last part of the input data printed out is all the trajectory-only input.
- 4. Program name and identification of the particular Aerospace version.
- 5. The Epoch time for this run.
- Indicators printed out giving the logical flow from segment to segment and old and new function numbers.
- 7. Card image of last END card in the deck.
- 8. Trajectory initial conditions in three coordinate systems. Initial-condition values as shown are the result of transformations which have been applied to the input values. The transformation for the input coordinate set (a. δ , β , A. r, v in this case) consists of conversion from decimal to octal numbers,

conversion of units from feet, degrees, and seconds to earth radii, radians, and minutes, and performance of corresponding inverse conversions for output. The two other types of elements sets also require accomplishment of coordinate-system transformations in addition to the number- and units-systems conversions noted above. Accuracy of the values as printed therefore is subject to numerical roundoff errors.

Ouantities in the left-hand column are position and velocity components in the basic vernal equinox coordinate system, with units of feet and of feet per second. The center column gives the usual ADBARV spherical system coordinates (i.e., Type-2 initial conditions in units of feet, feet per second, and degrees). The right-hand column from top to bottom contains orbit semi-major axis, eccentricity, inclination, right ascension of ascending node, argument of perigee, and time of last perigee passage in minutes from midnight of epoch day. Other units are feet and degrees.

- 9. Identification of atmosphere model to be used in computing drag force. LOCKHEED and ARDC 1959 refer to the Lockheed-Jacchia and the ARDC 1959 model atmospheres, respectively. Reciprocal of ballistic coefficient, CpA/W. Ballistic coefficient, W/CpA. d₁ and d₂ are values of certain constants in the Lockheed-Jacchia atmosphere density expressions.
- 10. The product GM, or the universal gravitational constant times the mass of the earth (frequently designated by μ), expressed in units of earth radii cubed per minute squared. Unitless coefficients of the zonal harmonic terms in the earth potential field expansion (i.e., J_2 through J_{15}). Coefficients and longitudinal arguments of tesseral and sectorial terms in earth potential field expansion, with J indicating a coefficient and L an argument in degrees. The digits following J or L are the

associated Legendre polynomial degree and order, respectively.

- 11. Names of solar-system bodies included in computation of perturbative accelerations. In this case none are used.
- 12. Trajectory method indicator. The Cowell formulation of the equations of motion is the only trajectory method available in the present TRACE-D program.

Numerical integration parameters. The Gauss-Jackson method (subroutine DEO2) is the only integration method available in the present TRACE-D program.

- 13. The indices N_1 and N_2 input in the IOB array respectively indicate the highest-degree zonal term and the highest-degree and -order tesseral term. No term higher than those indicated by these input numbers will be computed, regardless of the model coefficients and arguments that are input to the physical constants region.
- 14. Physical constants and units conversion factors. Decimal and octal equivalents are given for the following quantities.

a.	OMEGA	$E(\omega_e)$	Earth	rotat	ion	rate	in
			radian	s per	mi	nute,	

- b. ALPHA $G(\alpha_g)$ Right ascension of Greenwich at midnight of the day of epoch in radians,
- c. FT/KM Feet per kilometer,
- d. E.R/A.U. Earth radii per astronomical unit,
- e. I-O, DISTANCE Input/output units conversion factor in feet per earth radius,
- f. G Acceleration due to gravity in feet per second squared,
- g. DEG/SEC// Units conversion factor in RAD/MIN degrees per second/radians per minute,

h.	RELATIVE MASS (SUN)	Mass of sun relative to mass of earth,
i	(VENUS)	Mass of Venus relative to mass of earth,
j.	(JUPITER)	Mass of Jupiter relative to mass of earth,
k.	GM	Earth gravitational constant (μ) in earth radii cubed per minute squared,
1.	EARTH RADIUS-FT	Number of feet per earth radius for internal calculations (rather than I-0),
m.	N.M/E.R	Number of natuical miles per earth radius,
n.	I-O, VELOCITY	Conversion factor for input/ output in feet per second/ earth radii per minute,
n. o.	I-O, VELOCITY FT/SEC// E.R./MIN.	output in feet per second/
	FT/SEC//	output in feet per second/ earth radii per minute, Units conversion factor in feet per second/earth radii
0.	FT/SEC// E.R./MIN.	output in feet per second/ earth radii per minute, Units conversion factor in feet per second/earth radii per minute, Earth flattening (reciprocal
o.	FT/SEC// E.R./MIN. 1/EPS	output in feet per second/ earth radii per minute, Units conversion factor in feet per second/earth radii per minute, Earth flattening (reciprocal of earth ellipticity), Mass of moon relative to
o. p.	FT/SEC// E.R./MIN. 1/EPS (MOON)	output in feet per second/ earth radii per minute, Units conversion factor in feet per second/earth radii per minute, Earth flattening (reciprocal of earth ellipticity), Mass of moon relative to mass of earth, Mass of Mars relative to

- 15. Date and time of day (Greenwich Mean Time) with which the quantities in the print block following are to be associated.
- 16. Minutes from epoch, minutes from midnight of current day, system time (i.e., seconds from midnight of current day), and current integration step size in minutes.
- 17. x, y, z, r: Componenents and magnitude of the radius vector from geocenter to satellite in the basic coordinate system in units of feet.
- 18. \dot{x} , \dot{y} , \dot{z} , v: Components and magnitude of the inertial velocity vector with respect to the basic coordinate

- system in units of feet per second.
- 19. Geodetic latitude, in degrees, of the point where the radius vector intersects the ellipsoidal surface of the earth, geographic longitude measured east from Greenwich in degrees, altitude of the satellite above the oblate earth in natuical miles, and geodetic latitude of the subvehicle point in degrees. All latitude quantities are considered positive north of the equator and negative south of the equator.
- 20. α , δ , β , A: Right ascension of satellite position, declination of satellite position, flight path angle, and inertial azimuth of velocity vector in units of degrees.
- 21. Revolution number, nodal period in minutes, nodal period decay rate in minutes per revolution, and nodal regression rate in degrees per revolution. Due to the fact that the nodal period is calculated by simple subtraction of ascending-node crossing times, this quantity cannot be determined until two ascending node crossings have been detected. Also, since the nodal-period decay rate is computed by differencing the nodal-period values at successive ascending nodes, this rate cannot be calculated until three ascending nodes have been crossed. The nodal regression rate is computed by differencing values of right ascension at successive ascending nodes.

4.2 Observation Generation Sample Output

Figures 20 to 24 contain the output from the observation generation test case. There are numbered descriptions corresponding to the number codes on the output; however, only the output that has not been previously described in Section 4.1 is covered here. Therefore, Figures 20 and 21 are included for completeness but need no further description (see Section 4.1 for this information).

- 1. Bias inputs for data and last END card.
- 2. Sigmas. In the case of a data generation run, the sigma table is used for the purpose of sepcifying the standard deviation of random noise which is to be applied to the generated data. Interpretation of the printed output shown is otherwise the same as described under section for Data Generation.
- Station locations, latitude, longitude, and altitude.

4. Data Limit Specifications. The eight columns from left to right contain station identification, data interval, minimum elevation angle, maximum elevation angle, maximum range in nautical miles, and data-generation start and stop times in days, hours, and minutes from midnight of epoch day.

The information shown indicates that the following specifications have been given to the program:

- a. Observations are to be generated for station AA at 15-second intervals whenever the computed local elevation angle is above zero degrees.
- b. No maximum elevation angle is assumed and no maximum range is to be considered (data generated for all ranges and for all elevation angles greater than zero).
- c. Station AA is assumed to be active during the time interval from epoch until a time 24 hours after midnight of epoch day.

In the case of this particular data generation run, the corresponding Specification-I input items for Stations BB through FF are identical to those for Station AA. However, this need not be true in general, inasmuch as each station is independent of the others with respect to these input items.

- 5. Parameter indication. The message indicates that the range bias parameter has been selected for Station BB. In the case of a data generation run, radar parameters are selected only for the purpose of applying biases to the generated data, in this case a range bias on Station BB data. The message alluding to the correction of parameters therefore should be ignored.
- 6. Data Types. These headings define the format of the table appearing beneath them. The purpose of this table is to define the types of data which are to be generated for each station. Except for the station-identification column header, which is printed vertically, the headings appear in two horizontal rows, with the top row displaying the symbols RANGE on the left and LONG. on the right and the second row the symbols SUR.R on the left and U, V on the right. The individual headings are interpreted in accordance with the following:

Heading	Description or Symbol	Units
RANGE	Range	n mi
AZMTH	Local azimuth angle	deg
ELEV.	Local elevation angle	deg
R. DOT	Range rate	ft/sec
P. DOT	Range-rate difference	ft/sec
Q. DOT	Range-rate difference	ft/sec
P	Range difference	ft
Q	Range difference	ft
AZ. DT	Rate of change of local azimuth	deg/sec
E. DOT	Rate of change of local elevation	deg/sec
R. DDT	Second time derivative of range	ft/sec ²
MU. VIS	Mutual visibility	(indicator)
LAT	Latitude of sub-vehicle point	deg
LONG	Longitude of sub-vehicle point	deg
SUR. R	Surface range, station to sub- vehicle point	n mi
HIGHT	Altitude above oblate earth	n mi
DOPLR	Doppler frequency shift	cps
LOOK	Look angle	deg
VARI	Variances	Same as corresp. observations
KAPPA	Angle between radius vector and local vertical	deg
ASPCT	Aspect angles	deg
ATTEN	Signal attenuation	db
X, Y, Z	x, ŷ, ż	n mi
T-R, D	Topocentric right ascension and declination	deg
HR, ANG	Topocentric hour angle	deg
U, V	Horizon-scanner angles, u, v	deg

The two horizontal lines associated with each station are the line containing the station-identification symbol and the line immediately below it. An X on the first line of a Y on the second line indicate that the corresponding quantity as defined by the table header is to be generated. In the present example, the indicated data types for Station AA are range, azimuth, elevation, range rate, height (altitude), $\hat{\mathbf{x}}$, $\hat{\mathbf{y}}$, $\hat{\mathbf{z}}$, topocentric hour angle, and horizon-sensor angles u and v.

- 7. Segment transfer messages.
- 8. Rise message. The time when the satellite becomes visible from a particular station (at the specified minimum elevation angle) is obtained by interpolation and printed in the manner shown along with the local azimuth angle for the corresponding time.
- 9. Time corresponding to generated data. The time shown is to be associated with the data quantities appearing on the line to the right of the time printout and on the line following. The time is given both in hours (0 through 24) and minutes of the day as identified at the top of the output page, as well as in minutes from start (i.e., minutes from epoch). In the case of the particular output shown, time from start corresponds to the time of day because the epoch chosen for the run happened to be midnight.
- 10. Maximum elevation point. The time when the elevation angle reaches its maximum is obtained by interpolation and printed along with the corresponding values for the elevation and azimuth angles in the manner shown.
- 11. Set message. When the time at which the elevation angle reaches the specified minimum from above is obtained by interpolation, the print shown at this position occurs.
- 12. Duration message. After each pass, a message is printed giving the time in minutes during which the elevation angle was above the input minimum value and the range was below the input maximum value.

4.3 Orbit Determination Sample Output

This section contains the output from the orbit determination test case. Here also, only that output which has not been previously described is considered, although all of the output is shown in Figures 25 through 31.

- 1. The station location card quantities, refraction indicator, sigma set, latitude, longitude, and altitude.
- 2. Each line is the printout of one observation card. Given are the date, station ID, both the type and set number for these measurements, and the three measurements. In this case Line 1 has a Range Rate measurement only.
- 3. This line contains a Range measurement only.
- 4. Indicates those parameters chosen in input to be estimated.
- 5. In this case, the spherical set of initial conditions, drag coefficient, GM, J_2 and J_3 are to be estimated.
- 6. The number of iterations after which the program stops. In this case, one only.
- 7. A count of the parameters to be estimated.
- 8. A count of the number of observation cards read.
- 9. A total obtained by assuming three observations per cards.
- A count of all the sites entered on station location cards.
- 11. The number of locations that all the data has been packed into and then stored on scratch tape.
- 12. The number of flocks (TF and TR cards) read.
- 13. Segment transfer messages.
- 14. Differential correction bounds. This sequence corresponds to the previously described sequence of the parameter indications.
- 15. Weighting sigmas. The observation type number and the value of the weighting value are shown.
- 16. Definition of current orbit. For each iteration the current values for the parameters are used to compute the quantities shown
- 17. Node print. Each time the integrated trajectory crosses the equator (as determined by interpolation between integration steps) the date, time in minutes from midnight of epoch, and the rectangular elements (x, y, z, x, y, z,) in units

of earth radii and earth radii per minute are printed. The numerical integration interval for each satellite begins at epoch and ends at the time of the latest observation for that satellite. A message is printed each time any of the events of equator crossing, start of thrusting, end of thrusting, or orbit adjust are detected during the integration interval.

- 18. Station identification and system time of residuals. These are to be associated with all residuals which appear on the same line. It should be noted that system time is defined as seconds from midnight of the current day.
- 19. Residuals. These are unnormalized differences between the input observations (as modified by bias or refraction corrections) and corresponding values for the same observation types computed from the integrated trajectory position at the observation times. Up to six residuals for the same time are printed on one line. The observation type is indicated in parentheses immediately following the residual value in each case. Note that residuals appear for the unweighted as well as for the weighted observations.

Identification of the foregoing observation-type indicators with observation descriptions or symbols defined elsewhere in this report is in accordance with the following:

Indicator	Description or Symbol	Unit
R	Range	ft
A	Azimuth	deg
E	Elevation	deg
TR	Topocentric right ascension	deg
TD	Topocentric declination	deg
HA	Topocentric hour angle	deg
GR	Geocentric right ascension	deg
GD	Geocentric declination	deg
U	Horizon scanner in-plane angle	deg
V	Horizon scanner cross-plane angle	deg
Н	Altitude (h)	ft

Indicator	Description or Symbol	Unit
X	x	ft
Y	ŷ	ft
Z	ż	ft
R	Range	ft
P	Range difference	ft
Q	Range difference	ft
RD	Range rate	ft/sec
PD	Range-rate difference	ft/sec
QD	Range-rate difference	ft/sec

- 20. Observation time. The time identified in Item 2 in terms of seconds from midnight is given in alternate form, wherein the day of the month and the hour and minute of the day are given as integers and seconds are given to two decimal places.
- 21. RMS summary of residuals. The root-mean-square of the residuals for each type of observation from each station is computed by the residuals editor and the result is printed at this location. Included are the station identification, number of residuals included in the RMS (i.e., the total number for that station and type minus the number deleted by the editor on this iteration), RMS, and the RMS divided by input weighting sigma. The observation-type indicators are the same as those used in the residuals print output. Units are feet, degrees and seconds. Interpretation of the range-rate summary for station MH is that 206 range rate measurements were used to compute the rms which equals 1.61216 feet per second.
- 22. Iteration number. TRACE-D performs the tracking, or orbit determination function, by computing series of differential corrections to the parameters selected by the user. The iteration number is advanced each time the process of computing a set is repeated. The number may be interpreted as an indication of the number of times the trajectory-integration/least-squares process has been performed.
- 23. Observation count. The number of individual observations included in the current least-squares computation is indicated.

24. Convergence indicator. If the weighted RMS for all residuals for the current iteration is less than that for any previous iteration, then the fitting process is converging and the message shown is printed. If the RMS obtained on the current iteration is greater than the smallest RMS obtained on previous iterations, the message

CURRENT ITERATION IS NOT GOOD

(RMS = 0.xxxxxxxx xx)

is printed in this position.

25. Current solution. If the iteration is successful (i.e., the overall RMS has been lowered), indicated values are the parameter values used in the trajectory, partial derivative, and residuals computations which have just been completed. In the case of Iteration No. 1, they are the input values of the parameters.

If the iteration is bad, the words

GO BACK TO

are printed, and the values of the parameters which so far have produced the lowest RMS are recovered from memory and printed at this point. Parameter names are generally self-explanatory, with the possible exceptions of the multiple-vehicle elements. The satellite number is printed before the element name for Satellites 2 through 6.

- 26. Current solution in octal digits and machine units. These numbers corresponding to those described in Item 30 are given both in the octal mode and in the units used for internal computations. Use of these quantities permits bypassing units and number-system conversions during input and output.
- 27. RMS. This is the quantity which is to be minimized in the tracking or orbit determination process and is the root-mean-square of the normalized residuals included in the least-squares calculations on the current iteration.
- 28. Corrections. The result of solving the system of normal equations associated with the parameter which occupies the corresponding position in the current solution block. Units are feet, degrees, and seconds.
- 29. Bounds. Current values of the numbers used to limit the size of corrections. In general, these bounds are

automatically increased on a good iteration and automatically decreased on a bad one.

30. Bounding indicator. This message will be either

HITTING BOUNDS

or

NOT HITTING BOUNDS

The first message indicates that the magnitudes of the corrections have been controlled by solving the system in such a way that the constraint implied by the bounds is satisfied, and the latter that the normal equations have been solved without applying the bounds.

- 31. Next solution. Each value is the sum of the parameter value given in the corresponding position under "current solution" and the associated correction. These are the parameter values which will be used for the next solution.
- 32. Next solution in octal mode and units of earth radii, radians, and minutes.
- 33. Predicted RMS. If the fitting process is converging in a completely linear fashion, this will be the RMS on the next iteration. The comparison of this number with the current RMS (see Item 32) may be used to measure the degree to which the process has already converged.
- 34. Sigma of parameters divided by sigma of the normalized observations. The numbers given are the square roots of the diagonal elements of the inverse normal matrix. If certain assumptions are made about the characteristics of the observation set, the numbers may then be taken as the variances on the parameter solutions.
- 35. Correlation matrix, correlation coefficients for the parameter set. These values are computed directly from the covariance matrix (i.e., the inverse normal matrix). Rows and columns are in the same sequence as the Item 34 data.
- 36. This is the upper half of the normal matrix.
- 37. This is the lower half of the inverse normal matrix.

Migure 16. Trajectory Pradicates Output Listing of Input

BASIC INPUT CARD 1 BASIC INPUT CARD 2	BASIC INPUT CARD 3 BASIC INPUT CARD 4		BASIC INPUT CARD 9 BASIC INPUT CARD 1C BASIC INPUT CARD 11	BASIC INPUT CARD 12 BASIC INPUT CARD 13 BASIC INPUT CARD 14	BASIC INPUT CARD 15 BASIC INPUT CARD 16 BASIC INPUT CARD 17	BASIC INPUT CARD 18 BASIC INPUT CARD 19 BASIC INPUT CARD 2C	BASIC INPUT CARD 21 BASIC INPUT CARD 22 BASIC INPUT CARD 23	BASIC INPUT CARD 24 BASIC INPUT CARD 25 BASIC INPUT CARD 26	BASIC INPUT CARD 27 BASIC INPUT CARD 26 BASIC INPUT CARD 29	BASIC INPUT CARD 3C BASIC INPUT CARD 31
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BASIC INPUT CARD 32	BASIC INPUT CARD 33	BASIC INPUT CARD 34	BASIC INPUT CARD 35	BASIC INPUT CARD 36	BASIC INPUT CARD 37	BASIC INPUT CARD 38	BASIC INPUT CARD 39	BASIC INPUT CARD 4C	BASIC INPUT CARD 41	BASIC INPUT CARD 42	BASIC INPUT CARD 43	BASIC INPUT CARD 44	BASIC INPUT CARD 45	BASIC INPUT CARD 46	BASIC INPUT CARD 47	BASIC INPUT CARD 48	BASIC INPUT CARD 49	BASIC INPUT CARD 5C	BASIC INPUT CARD 51	BASIC INPUT CARD 52	BASIC INPUT CARD 53	BASIC INPUT CARD 54	BASIC INPUT CARD 55	BASIC INPUT CARD 56	BASIC INPUT CARD 57	BASIC INPUT CARD 56	BASIC INPUT CARD 59	BASIC INPUT CARD 60	BASIC INPUT CARD 61	BASIC INPUT CARD 62	BASIC INPUT CARD 63	BASIC INPUT CARD 64
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2 -6	*1088012 -6	1- 4694924.	6- 61077744.	35430592 -8	.2052417 J1	.2771455 -9	.3416347 J2	- 1746101.	.3251625 -7		•3549629 J9		-1974783 KI	i 93759£i.		7.623267	31,73482	169,9065	876	47.13021	273	859865*8	66601	19.70539	3308.608	164,1975		9.804658	10277		0848	
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1 9-	-6 11	-8 15	-8 19	-1 23	J0 27	-9 31	J2 35	34 45	JO 55	81	96 9f	0 ¥	401 6F	JB 116		3	•	11	15	19	23	21	31	35	5+	\$3		06	Ħ		*	
.7017339	*1111605	+1507404	.1967936	.3972437	*1515140	.3762496	.1641761	.8609215	.7857074	2783799	.1717906	.1059143	1326684	.5398041		165,2042	219,3494	232,5121	56.95252	66.23621	12.06147	27.20422	57,94327	15.09665	13.95194	59.07748	14.87681	11-44440	30.31227	15.65423	6. 108.4	
9	10	•	18		26		*	* **	48	. 11	• 68	101	102	113	0811		6 2			18 6	22 1		30 8		100	\$ 84		1 68			117 16.80139	S HILLS

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2 25-5	BASIC INPUT CARD	17	
	BASIC INPUT CARD	68	
4 47.18	BASIC INPUT CARD	59	
5 22999226.	BASIC INPUT CARD	70	
797.530	BASIC INPUT CARD	71	
	BASIC INPUT CARD	72	
12 1 3 0 4 5.	BASIC INPUT CARD	73	
5 60.	BASIC INPUT CARD	74	
4 30.	BASIC INPUT CARD	. 51	
DRAG DOB	BASIC INPUT CARD	76	
12 1	BASIC INPUT CARD	7.7	
3 6.83 4 -15.684	BASIC INPUT CARD	7.8	
TYEAR 1967 IHNIH 7	BASIC INPUT CARD	51	
IDAY 8 TZNE 0.	BASIC INPUT CARD	96	
HR 15, HIN 0, SEC 0,	BASIC INPUT CARD	81	
DPRCDEX, X	BASIC INPUT CARD	82	
	BASIC INPUT CARD	83	
END	BASIC INPUT CARD		

Figure 16 Goot. 1

17 _{p.3} Beader Page CUCCCCCCC CUCCCCCCCC CUCCCCCCCCCCC	AA + CCCCCCCCC EEEEEEEEEE *** TRACE-D (ADOLAD) *** HCC. NUMBERS 1.2 (4)	000° 000° 000° 000°	3 FUNCTION 15	FUNCTION IS 3			
# ####################################	RR + AA + + + + + + + + + + + + + + + +	YEAR MONTH DAY TECNE HOUR	OLD FUNCTION IS O NEW FUNCTION IS O NEW FUNCTION IS O NEW FUNCTION	CANE TAUM SEGMENT OF ARE IN SEGMENT			
* -		НЭОСН	12.18.46 BEGIN				

						(10)				
BASIC INPUT CARO 1 (7)		07813E+08 68993E-02 44384E+02 18841E+02 21554E+02 13988E+03			.20987600E+03 .14023820E+03 .50046990E+02 .647130210E+02 .42588280E+02		14876810F+	300000000 = 6 3000000000 = 6 3000000000 = 8 44 3000000000 = 6	11	300000000°
BASIC I		A= .23107813E+08 E= .77068993E-02 I= .345384E+02 O= .2311664E+02 U= .1772154E+02 T= .81613999E+03	-12500000E+03	00000E-05 J5 00000E-07 J10 00000E-06 J1 [53= [53= [54= [55=	.42640940E-07	.000000000 00 112 5= .000000000 00 112 6= .000000000 00 112 7= .000000000 00 112 9=	888888888888888888888888888888888888888	000000	.00000000E 00 [1310= .1717966E=18 [1312= .35496290E-19 [1313= .83605890E-08 [14 1= .0000000E 00 [14 2=	
	INITIAL CONDITIONS	2550000E+03 2550000E+02 .90350000E+02 .47180000E+02 .22999226E+08	00000E+02 W/CD 00000E+01 D2 RTH MODEL	25460000E-0527000000E-0611400000E-0 00 J53* -03 J54* -03 J55*	070E+02 J61= 940E+03 J62= R20E+02 J63= 170E+03 J64= 110E+03 J65= 210E+03 J66=	8374930E+02 2061470E+02 3727300E+01 3465920E+02	720%220E+02 J121 5920%260E+01 J121 5920%260E+01 J121 5920%270E+02 J13 5809930E+02 J13	2837470E+02 5510010E+02 9705590E+02 8560140E+01 8550140E+01	0000000E 00 0000000E 00 0000000E 00 0000000E 00	3951940E+02 J14 5= 0980560E+03 J14 5= 6256360E+02 J14 5= 0077480E+07 J16 7=
		0E+08 ALPHA= 7E+06 DELTA= 0E+07 BE1A = 3E+04 AZ = 8E+05 R = 8E+05 V =	10	.10826450 33300000 4570000 [21= [31= [32= [32=	133= 141= 142= 142= 143= 143= 143= 143= 143= 143= 143= 143	17 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2	1 8 5 = 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2 6 7 000 0 6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	86092150E-14 L 9 9= .1 -10134710E-06 L10 1= .3 -11739520E-09 L10 3= .6 -11739520E-09 L10 3= .6
		X = .20748520E+08 Y = .65204847E+06 Y = .99014220E+07 XD07= .75671283E+04 YD07= .17953858E+05	T.WD	6M 55303706-02 J2= J6 646000006-06 J7= J11 202000006-06 J2- J22 15598006 05 J32 15598006 05 J32 310842906-05 J32 310842906-05	J33= ,23905980E-06 J41= ;70173390E-06 J42= ;16520006-06 J43= ;2109120E-09 J44= ;49869920E-08 J51= ;11116050E-06		J 7 6= .15151400E-10 J 7 7= .20524170E-11 J 8 1= .6870100E-05 J 8 3= .3669090E-08 J 8 4= .27714550E-09	J 8 5= .23413300E-10 J 8 7= .1841016-12 J 8 7= .1841016-12 J 8 1= .33183470E-12 J 9 1= .76423820E-09		19 9= .8602150E-14 110 1= .10134710E-06 110 2= .4724120E-08 110 3= .41739520E-09

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ALPHA, DELTA, BETA, A 120, 83651095) 48, 25372594 48, 25372323 98, 57732323	ALPHA, DELIA, BEIA, A 146,43077687 43,35092053 89,55149561 114,38479712	ALPHA, DELTA, BETA, A 166, 59726815 33.86722360 89.57441311 127.11199948	ALPHA, DELTA, BETA, A 182, 19590890 21, 85679475 89, 645C786	ALPHA 1	ALPHA,DELTA,BETA,A 202,9555504 00000299 89,83657563 138,55663441	ALPHA, DELTA, BETA, A 201-26480397 201-36480397 89-88918664 138-37283634 FUNCTION IS 0	O FUNCTION IS 0
SEC. (18), CONG.H.SBV 26.05 (18), 20, 10, 10, 10, 10, 10, 10, 10, 10, 10, 1	LATTLONGTHYSBV 65 43.554303 05 345.52577 04 363.35710 05 43.52467	SEC. LAT, LONG, H, SBY 1E+05 34,04550 66+05 74,43884 6E+05 370,87110 1E+05 34,02811	1AT-LUMG-H-SBV 04 22-00012 18.78406 05 377-23886 05 21-98690	LATTE	LAT,LONC,H,SBV 04 -000000 105 37,48365 05 384,82785 05 384,82785	SEC. LAT,LONG,H,SBV 3E-04 -4.90010 EE-05 41.34611 EE-05 385.94442 5E-05 385.9445 5E-05 1N SEGMENT 13 NEW FUNCTION IS ARE IN SEGMENT 62	NEW FUNCTION IS ARE IN SEGMENT 63
00000 - xD01.v xD01.v xD01.v xD01.γ (1.009559 (1.009559 (1.009559 (1.009559 (1.009559 (1.00959 (1.0	X001.W X001.W X001.W 0818373776E405 0714783492E405 0872765022E404 08 .24679845E+05	00000. XD01.V 1275336 1714717 1223455	XXD01.V XD01.V 0858797845E+04 061776552E+05 07159775655E+05 0724577597756	0000 0001. .1550721 1660430 1860017 1860017	7. 12.34578 SEC. XDD1.V 08 .62654795E+04 0714971745E+05 0118360968E+05 08 .24520795E+05	00000 SE XD01,V .819983934 182451616 1824516165 18246161 245138736 SEGMENT 31 A SEGMENT 13 A	3 H
X, R X, R X, R 1 786474395+07 0 (16) 171927915+08 0 (20) 171927915+08	7 15 HRS. 40 MIN. K**R 1	7 15 HRS. 45 MIN. KAR 18 T04571E+08 18 T04571E+08 18 T04571E+08 18 T04571E+08 18 T04571E+08	7 15 185, 50 MIN. X+R 0 -215225245+08 0 -82527309E+06 0 -82527309E+06 0 -82527309E+06	<u>.</u>	7 15 HRS, 58 HIN. 1 X,R LE	7 16 HRS. 0 MIN	- CAME FROM SEGME
7/ 8/67 NE, MM, ST, DT 35, 00000 935, 00000 56100, 00000 2,00000	7/ 8/67 HE,MM,51,01 40,00000 940,00000 56400,00000	1, 8/67 ME.MM.ST.01 45.00000 945.00000 56700.00000	7/ 8/67 86.7MH.51.D1 50.00000 950.00000 57000.00000	## ###################################	77 8767 ME, MM, ST, DT 58.20576 958.20576 57492, 34578 2.00000	7/8/67 ME,MM,ST,DT 60,00000 960,00000 57600,00000	

Figure 19. Rphameria Output Gast 25 minutes of output]

Figure 20. Observation Generation Output Listing of input

, I	IRD 2	, 08	IRD 5	NO 6	IRD 8	ND 9 ND 16	IRD 11	MO 12	146 14	CARD 16	IRO 17	NO 18 1	ARD 2G	IRC 21 IRD 22	ARD: 23	RD 24	IRO 26	#B. 17	RO 20	IRO 29		80 J
STATE INPUT CIND	BASIC INPUT CARD	BASIC INPUT CARD	BASIC INPUT CARD	BASIC INPUT CARD BASIC INPUT CARD	BASIC INPUT CARD	BASIC INPUT CARD BASIC INPUT CARD	BASIC INPUT CARD	BASIC INPUT CARD BASIC INPUT CARD	BASIC INPUT CARE	MATTE INPUT CARD	BASIC INPUT CARD	BASIC INPUT CARD	BASIC INPUT CARD	BASIC INPUT CARD BASIC INPUT CARD	10/15/65 BASIC INPUT CARD	BASIC INFUT CARD BASIC INFUT CARD	BASIC INPUT CARO	BASIC INPUT CARD	BASIC INPUT CARD	BASIC INPUT CARO	BASIC INPUT CARD	BASIC INPUT CARD
JEWOLEN EIN GESTEUR FUNDERWITE	2 13 0	-9 26 1 30 L	32 64 33 1	135 1 37 .001 10 2820.1763 141 1		5. 85- 0150558, 5 5- 884528164, 8	10 10	14 57,2957795 15 20923736 17 .0122999 18 .814979	20 317.887 24 95.129	26 32-174 30 318762-3	32 1.0471976 33 3.14159265	35 300000, 36 82505,922	3 6.83	-	STANDARD DECK FOR GUIERS 6, TH ORDER EARTH MODEL	.19727926 -2 15 -2 15 2045051 -2 1-20451741. 2 - 657:1 2 1.00-1.	, .4482 -6 5 .1643 -6	9- 61250° 8'9- 9851°	- 45550. 11 9611. 0	13 .004093 -6 14 .0008462 -6	4- 6110. TJ 4- 64160. 61	-6 19 .0001128 -6 20 .0000519 -6
EL TANGE TANGE OF TANGE	11 1 12		31 .015625 3	134 4 135 18 0. 40	39	5 2-+00-92575\$• 1	:	13 3280.8399 14	19 .107821 2	25 MINES 2	31. 1.5	34 298,3 TMATX4	DRAG .01 12	KREFCI.	GC STANDARD DECK	1-509251110	3 1.856 -6 4	. 4278 -6.T	9 - 18/400* ¥	12 .005842 -6 13	115 .06611 -6 16	18 .002256, -6

2.2	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	ui ni	90		3¢	4.1		**		47		20	52	m.c.		56		5.9	
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Figure 20. (Cont.)	ř.				•											605			
5.31	-136,68	-3.45	12.11.61		-1,56	6	•									•05	1,000		
e	~ •	12	15 157	2680	9 1	-61108	9 41 1 HNUH 2							18		ın			
-13.18	16,00	-2.60 +	-15:32	-14.34	-2.693	.210	13 ; 1YEAR 1985			•06	Ī			_	- Pa	•05	1000.		
2	w sc	11	4	20,	6 4	H	I3 IYEAR			8			1 1 2	17	at ott	*			
-	4 -151.03 7 - 27.44	-81.86	13 58.25	-17.75	2 1082,76 -6 3	.0		23	-10 - 10 - 10 - 10 - 10 - 10 - 10 - 10	•		PE4	1351044	9	19 13 110 14 112 119 - ATCHAIGG.	7			
0817		10	112	19	•	60	4 5	IDAY	2	2	4	IPTAPE4		91	4 2	3		END	

Figure 21: Masder Page		AAA + AAAA + AAAAAA	* AAAAAAAAAA	TRACE_D (AD014D) ***********************************	ONTH GAY TZONE HOUR NIN SEC. 2. 23000 .000	CITON IS 0 NEW FUNCTION IS 4 FUNCTION IS 4 CITON IS 0 NEW FUNCTION IS 4	OM SEGNĘNT 62 ARE IN SEGMENT 2 FUNCTION IS 4			
	4	EE			YEAR HOWIN GAY 1965. 2. 23.	CANE FROM SEGNENT 63 OCLD FUNCTION IS 0	FROM SEGMENT			

	2		.500006CE-01)(2)			3.3 8.0				411	23540
BASIC INPUT CARD	BASIC INPUT CARD	BASIC INPUT CARD	\$ *50000000E-01 6	.21533353E+08 .35865344E-09 .6500000E+02 .90005516FE+02 -960145701E+02	CE+03 OE+02	75	L52=260C0CC0E+01 L53=3450C00E+01 L54=1535CC0E+02 L55=1532CG0E+02 L61= .1572CG0E+03 L62= .11315CG0E+03 L63=175CGCE+03	L64= .60740CCCE+02 L65=1775GGGE+02 L66=1434GGGE+02		COWELL STEP TO RUNGE KUTTA FF=6400E+02	-5530\$505E-02 620017123540
			*10000000E-00 4 *5000000E-01	### CONDITIONS ###################################)E-01 W/CDA = .1000000CE+03	0000E-05 34= -	J52= .53290000E-07 J53= .58420000E-08 J55= .40930000E-08 J51= .66110000E-07 J62= .3746000E-07 J63= .1166000E-07	0E+01 J64= .22560000E-08 0E+02 J65= .33280000E-09 0E+02 J66= .51530000E-10 PERTURBATIONS		19 A= 1.COO RATIC OF COWELL (= .1562E-01 MAXIMUP=	CCNSTANTS 10 GM
	(1) (1) (2)		\$16MA TABLE .1000000E-00 3 .1000	ALPHA- DELTA- BETA = AZ = R = Y =	CDA/W = .1000C00CE-01 D1 = .6830000E+01	.10827600E-02 J3= 6330000E-06 J8=	121= .00000000E 00 122=13180000E+02 131= .53100000E+01 132= .15000000E+02 133= .16000000E+02 141=13680000E+02 142= .27470000E+02	888	UF MOTION)	SUBRUUTINE SON E BAR* .1000E-09 A.* .1000E-01 URBATIONS FOR CORRECTOR USE NI = 9 NZ* 6	HAL 26956-02 7105E+01
HRAPARDS, 99	DO1,0188 RBIAS 03,01	DQ.	1 .1000000E+03 2	X =10056004E407 Y = .2150986DE+08 Z = .00000000 0 XOOT =10793656E+05 XOOT =50461966E+03 ZDOT = .23172351E+05	ATMOSPHERE - LOCKHEED	5304505E-02	J21= .00000000E 00 J22= .1723000E-05 J32= .4482000E-06 J41= .72780000E-06 J42= .1536000E-06	IMO	FORMULATION COWELL (EQS.UF MOTION)	DIFFERENTIAL EQUATION SUBRUUTINE GAUSS-JACKSON STEP SIZE - INITIAL - JUDUDE-61 DO NOT RECOMPUTE PERTIRBATIONS FOR CORREC FOURTIONS OF MOTION USE NI = 9 NZ= 6	

4 455000CC000 4 74003215600 5 223146314620 5 223146314620 3 314631463146 1 412076346600 2 2323222700 2 30446727270							
- FT 20925741E+C 34439336E+O 34876230E+C 2993900E+C 12299900E+O 10762160E+O	FUNCTION IS 4	FUNCTION IS 4 FUNCTION IS 4				•	
353733740 EARTH RADIUS 605075320 N.M./E.R. 605060000 I—0, VELUCITY 671260166 FIZEC7FE.R.F 250716340 I/EPS. 146314620 (MOUN) 33752020 (MAUS)	ARE IN SECRENT 62 F NEW FUNCTION IS 4	NEM FUNCTION IS 6. ARE IN SEGMENT 12 F	•		Figure 22 (cont.)		
.32808399E+04 3403537 .23454865E+05 565000 .2092741E+08 4550000 .329273E+0E+0E 132071E .3293130E+06 7231463 .8149790CE+00 3553375 .317847C0E+03 4223351	CAME FROM SEGMENT 2 A	FRUM SEGMENT 62 A UNCTION ES 4 FRUM SEGMENT 1 A					
FT/KH E.R./A.U. I-O, DISTANCE G DEG/SEC//KAD/MIN RELATIVE MASSISUN) (VENUS)	3	14.36.56 BEGIN EXECUTION CAME ULD FI 14.36.58 BEGIN EXECUTION CAME					

Figure 23. Data Specifications

Figure 23. Data Specifications	. LATITUDE	. 75.00000000 300.00000000 1000.0000 1000.0000 1000.0000 1000.0000 100.0000	HIN.EL HAX.EL MAX.RANGE HDT START DEG. DEG. N.M MIN. DA HR MN DA HR MN	AZHTH ELEV. R.DOT P.DOT Q.DOT P Q AZ.DT E.DOT R.DDT MU.VIS LAT. LONG.	HIGHT DOPLR LOOK VARI. KAPPA ASPCT ATTEN X,Y,Z T-R,C G-R,D HR.ANG. U,V X X X X Y Y Y Y Y	x	(9) X X X X X X X X X X X X X X X X X X X	CAME FROM SEGMENT 12 ARE IN SEGMENT 1 FUNCTION IS 4 ULD FUNCTION IS 4 NEW FUNCTION IS 4 OLD FUNCTION IS 4 NEW FUNCTION IS 4 OLD FUNCTION IS 4 NEW FUNCTION IS 4 OLD FUNCTION IS 4 NEW FUNCTION IS 4
	ATIONS \$16 REF		=======================================			_		

Figure 24. Generated Data

ILC YARDS	3125.509 3137.836 3137.836 3148.852	3168.371 3176,608 3184.295 3190.240	3122.351 3134.880 3146.351 3156.854 3166.334	3182.736 3188.946 3194.411 3198.845 3202.239
0 6		EES (10) -1010-412 -054,212 -054,212 -054,212 -041,513 -041,573 -041,573 -041,573 -041,573 -041,573	=1572*426 -1531*189 -1531*189 -1546*138 -1546*138 -1546*139 -1466*139	-1318-244 -1318-244 -1274-715 -1274-715 -1230-643 -1230-643 -1230-643 -1230-643 -1230-643 -1230-643 -1230-643 -1230-643 -1142-031 -1142-031
HEIGHT X YARDS KIL Y YARDS KIL B HR.ANG U U CEGREES	1088-808 1113-590 1113-590 1113-590 1138-030 182-830 78-083 1162-830 196-511 80-126	AZIMUTH 142,251 DEGREES 105,467 1210,878 -10 317,202 81,148 105,463 1234,504 -9 312,920 82,170 105,455 1257,468 -8 308,742 1280,617 -8 304,604 84,214 AZIMUTH 122,587 DEGREES	105.313 552.279 =1 22.507 76.822 18.798 77.844 18.798 77.844 18.798 639.448 =1 18.7916 78.866 10.661 77.8888 105.347 77.8888 105.351 725.885 =1 18.351 725.885 =1 18.351 725.885 =1 18.351 725.885 =1	
HEIGHT GMYY YARCS TOP HR ANG CEGREES	105.410 336.501 105.431 336.505 105.447 330.236 105.458 105.458 321.512	AZIMUTH 1 105.463 105.463 125.920 105.455 308.442 304.604 AZIMUTH 1	105.313 22.507 22.507 105.330 105.330 105.340 105.340 105.340 105.340 105.340	105.340 105.340 356.136 105.327 350.827 105.424 AZIMIH 163 105.287 3105.287 3105.287 3105.287 3105.287
ANGE RATE FI/SEC ED DECLIN DEGREES	1901213 H 190121	15.76 MINUTES .426 1790.209 .906 63.560 .129 5566.645 .998 5325.267 .445 64.068 .955 6981.888 .705 64.271	42.80 MINUTES 1.144 -15084.728 1.359 -13902.781 5.006 62.371 1.920 -12552.291 6.935 62.628 6.935 62.628 7.140 63.053 3.001 -9308.496 1.202 63.546	388 -5164.263 646 -64.027 035 -3185.517 849 -64.277 968 -926.626 214 -64.562 45.10 HINUTES 007 1356.185 564 364.754 867 3604.314 948 -64.874
ELEVATION RA DEGREES GED RI.ASC GE DEGREES	### W - S - # # B	164 164 168 168	1.144 1.154 1.155,006 1.359 1.	163-386 163-386 165-646 4-035 167-849 170-214 170-214 170-214 170-214 170-214 170-214 170-214 170-214
AZIMUTH DEGREES DEGREES DEGREES	159,154 13,036 155,194 13,140 151,007 151,007 146,640 146,640 146,640 146,340	137, 939 -10, 380 -13, 652 -9, 690 129, 605 -9, 039 125, 807 -8, 465	201.704 -13.467 198.354 -13.154 -12.736 -12.442 -12.442 -12.442	
MANGE QM:Y YARDS TOP RT.ASC T DEGREES	645.973 162.791 830.615 167.047 819.452 171.310 812.601 175.780 810.253 180.152	6.00 812.477 137 6.00 812.477 137 184.587 -10 184.587 133 188.951 -9 6.50 830.117 129 6.75 845.334 125 197.394 -8 197.394 -8 197.394 -8 197.394 -8	3.00 BEGREES ELEV.1 3.25 141.179 3.25 791.759 145.814 3.50 759.095 2.75 78.710 3.75 759.095 4.00 704.815	84.75 668.364 84.75 668.364 167.824 167.824 167.824 173.208 85.00 652.696 178.739 4.25 DEGREES ELEV. 185.25 653.199 185.50 659.353 185.50 659.353
15-1	195-80 195-80 195-50 195-50	1.73 DEG 196.00 196.25 196.50 196.75 .00 DEG	28 28 28 28 28 28 28 28 28 28 28 28 28 2	
ST HR MINS		AA MAX EL (1 AA 3. 16.25 19 AA 3. 16.25 19 AA 3. 16.75 19 AA 3. 16.75 19 AA 3. 16.75 19		AA 4. 44.75 AA 4. 45.00 AA 4. 45.00 AA 5. 45.25 AA 4. 45.25

				100						
-	ST	RANGE M.Y YARDS	AZ IMUTH DEGREES	ELEVATION DEGREES	RANGE RATE	CM.Y YARES	Y KILO YARES P	KILO YARUS	TOP RT.ASC DEGREES	
201		TOP DECLIN (GEO RT. ASC DECRETS	GEC DECLIN DEGREES	TOP HR. ANG	DEGREES	PEGREES	DEGREES		
•	OO DEGREE	S ELEV.	· , I	HOURS 33.1	.11 MINUTES	AZIMUTH 1	49.915 DEGREE	EES		
273	174	824,583	148,101	146.	-14120,608	-1090,503	-2761.350	1931,605	142,384	
273		791.225	109.545	1.382	318.75	-1052.616	13 4	1976.559	146.073	
273	3.75	-34.273	110.342	33.831	315.185	38.011	52.849	2020.881	149.823	
		-31.768	110.856	34.761	311.506	6	53.463			
17	2 '	734-923	111.499	35.634	307.717	40.053	54.052	21004+400	1534086	
517	4	-26.147	112.253	36.483	303.912	41	54.617	666.0012	121.420	
274	274.50	695.282	127.075	37.453	-6136.014	-897.994	-2666.067	2151.478	161.617	
274	274.75	682.671	121.944	3.273	-4078.574	-858,816	-2644.261	2193,127	165,633	
37.6	00.576	475-241	113.480	36.209	295.850	43,116	55.675	2234.590	169.611	
	73 050	-16.110		39.	3	44.137	1			
275	275.25	673.200	111.575	3.539	E	m	-2599.453 2275.21	2275.219	173.764	
37.6	275.50	-12.624	114,980	190*0*	287,876	45.158	56.648	2315.230	177.842	
		-9.039	115.767	40.858	283.914	46.179	57.103			
215	51.5	-5.685	101.208	41.678	280.135	47.200	57.540	2354.111	181.731	
276	276.00	699.155	96.345	2.951	6626.616	-657.093	-2526.583	2392.713	185,522	
276	**25	717.894	91.502	2,695	0510.012	-615.847	-2500.517	2430.301	189,163	
276.	05.50	741.082	87.009	2.224	10248.754	-574.153	-2473.836	2467.506	192.671	
276	57.5	3.582	118.931	44.102	269.398	50.263	58.744	2503.773	196.169	
1112	00.1		119.796	1.125	13198.797	51,285	59,111	2538.768	199.309	
14.6		8.378	120.652	45.792	262.762	52.306	59.464	2573 140	762 202	
17	1		121.607	46.588	259.860		59.801			
BB SET (CLAPSED VISIBLE	.00 DEGREES	REES ELEV.)	INUTES 4.	HOURS 37.38	S MINUTES	. AZIMUTH	73.682 DEGREES	165		
	.00 DEGREES	REES ELEV.)	.9	HOURS 1.85	35 MINUTES	AZIMUTH 2	228.700 CEGRE	EES		
36	362,00	808.339	229.231	1.304	-23616,336	-1939.24	-2134,200	2055.880	65.177	
362	7.25	750.146	230.414	1.911	-23518.703	-18	-2130.351	2089.512	65.049	
1		-25.454	111.879	36.375	58.453	40.856	54.501	2162 603	711 77	
362	5.50	692.213	112.497	3.312	-23387,981 58,698		-2126.213	2142.083	04.1/4	
36	362.75	634.744	233.061	4.435	-23212.145	-1807,965	-2122.050	2184.493	94*520	

Pigure 25. Orbit Determination Output Listing of Input

		. •		•	5		12	13	14	15	. 91	11	1.8	61	3¢	2.1	2.2	23	24	25	2.6	27	2.6	5.6	3 C	11	*
	BASIC INPUT CARD	BASIC INPUT CARD	BASIC INPUT CARD	BASIC INPUT CARD	BASIC INPUT CARD	INPUT	BASIC INPUT CARD	BASIC INPUT CARD	BASIC INPUT CARD	BASIC INPUT CARD	BASIC INPUT CARB	BASIC INPUT CARD	BASIC INPUT CARD		BASIC INPUT CARD	BASIC INPUT CARG	BASIC INPUT CARO	BASIC INPUT CARD	46256 INDUSTRANT								
TRACE-D STANDARD INTEGRATION CON	.1 -9	1 31 .015625 32 64 33 1 -7	4 135 1 37 ,0001 38 0,	2820,18012 141 1	TRACE-D STANDARD PHYSICAL CONSTANTS 1C/ 1/65 .437526904-2 2 .55304203 -2 6 .5		13 3280,8399 14 57,2957795 15 20925738	16 332951.3 17 .01229853 18 .814979 .	19 .107821 20 317.887 21 95.129	23454.865 23 3443.93355 24 20925738	25 348762.3 26 32.174 , 30 348762.3	1+5 32 1.0471976 33 3414159265	298.3 35 300000. 36 82505.922	NUMB 42 3443,9336	0111N 12	DPRCDE X X	TIGTY92	1C 23.11454	26,51516	89.88977	45.13312	24780836.7	23765;259	- MAXIII	IYEAR 1967	THUM!	IntY 6

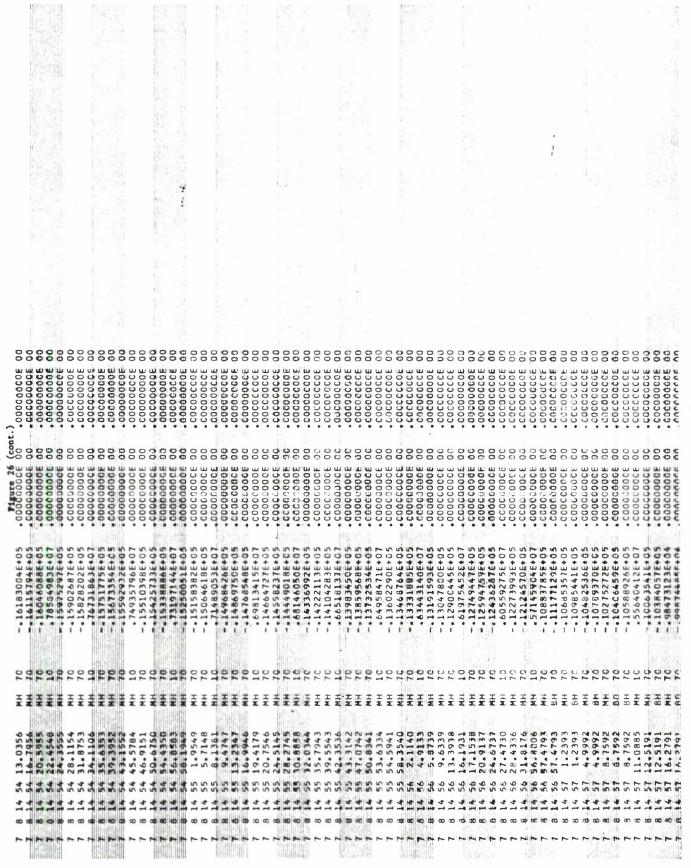
T2NE 0 Figure 25 (cont.)	BASIC INPUT CARO 33
HR 14.	BASIC INPUT CARD 34
MIN - 45,	BASIC INPUT CARO 35
DRAG .2849 12 1	BASIC INPUT CARG 36
. કે. કે. કે. કે. કે. કેલ કે. કે. કેલ કેલ કે. કે. કેલ	BASIC INPUT CARD 27
1108 10 12 6 13 10	BASIC IMPUT CARD 38
14 6	BASIC INPUT CARD 29
7790	ISIC INPUT CARD 40
210826452	BASIC IMPUT CARD 41
32546000 -5	BASIC INPUT CARD 42
4 -1,649 -6	BASIC INPUT CARD 43
5 210 6 6 . 646 6 7 333 6	BASIC INPUT CARD 44
B270 -69053 -610054 -6	BASIC INPUT CARO 45
08JT 2 1,5664 -6 3 1,7287 -6	BASIC INPUT CARD 46
4 .3025 -6 5 .1966 -6 6 .5234 -6	BASIC INPUT CARU 41
7 .1372 -6 8 .04166 -6 9 .009378 -6	BASIC INPUT CARD 48
10 ,12476 11 ,055466 12 ,022196	BASIC INPUT CARD 49
13 ,001605 -6 14 ,001029 -6 15 ,09572 -6	BASIC INPUT CARD SC
16 .02928 -6 17 .001037 -6 18 .0015006	BASIC INPUT CARO 51
19 ,000381 -6 20 ,000140 -6	BASIC INPUT CARD 52
08LT 2 ~15.5C 3 ~1.43	BASIC INPUT CARO 53
4 -32,30 5 32,31 6 -133,53	BASIC INPUT CARD 54
7 35,75 6 -2,75 9 26,09	BASIC INPUT CARD 55 BASIC INPUT CARD 54
32.27 14 -15.79 15 99	
-38.87 IT	BASIC IMPUT CARD 58
19 -25-28 20 -16-92	BASIC INPUT CARD 55
SIGMA22.96	BASIC INPUT CARO &C
2 .06056 \$ 22.96	BASIC INPUT CARD 61 BASIC INPUT CARD 62
4 .06056	BASIC INPUT CARO 63

5 22.96	Figure 25 (cont.)	BASIC INPUT CARD	6.4
95030 9		BASIC INPUT CARD	u,
		BASIC INPUT CARD	99
11516 101		BASIC INPUT CARD	6.7
		BASIC INPUT CARD	OU VO
		BASIC INPUT CARD	59
14 219		BASIC INPUT CARD	10
		BASIC INPUT CARD	11
16 319		BASIC INPUT CARD	72
DCPRAM2XXXXX		BASIC INPUT CARD	73
DOPRAHXXXX		BASIC INPUT CARD	11
		BASIC INPUT CARD	18
2 1.5		BASIC INPUT CARD	76
3		BASIC INPUT CARD	T.
		BASIC INPUT CARD	76
5 4920.		BASIC INPUT CARD	31
		BASIC INPUT CARE	90
•		BASIC INPUT CARD	6.1
B .1 -7		BASIC INPUT CARD	82
	•	BASIC INPUT CARD	E 8
		BASIC INPUT CARD	84
END		BASIC INPUT CARD	8.5

i dent

Figure 26. Reader and Observations

33 33 33 33 33 33 33 33 33 33 33 33 33	33333333333333333333333333333333333333									
++++ Pigura 26. Reader and Observations ++++ ++++ ++++ 1111111111 RERRRRRR + + CCCCCCCCC Effet 111111111 HRRRRRRR + + CCCCCCCCC FFFF	* AA AA + CC * AAAAAAAAA	+++ +++ TRACE-D (ADD14D) ++++ +++	EPOCH YEAR HONTH DAY TEONE HOUR HIN SEC 1967. 7. 8. 14. 45.000 .C00	OLD FUNCTION IS O NEW FUNCTION IS 1 CAME FROM SEGMENT 4.3 ARE IN SEGMENT 6.2 FUNCTION IS 1 OLD FUNCTION IS 0 NEW FUNCTION IS 1 INCOME OF BEGIN SAFETY OF SEGMENT 6.2 ARE IN SEGMENT I FUNCTION IS 1 OLD FUNCTION IS 1	ACTIVE EXECUTION CAME FROM SEGMENT 1 ARE IN SEGME	SIG REF LATITUDE LUNGITUDE HEIGHT HI	ATLONS HR HM SEC STA TYP 14 53 16.7706 NH 7017007600E-05 .0000000E 00 .0000000E 14 53 16.7706 NH 7016953515E-05 .0000000E 00 .0000000E 14 53 11.2185 NH 7016953515E-05 .0000000E 00 .0000000E	888888888888888888888888888888888888888	53 50.2880 MH 7016554961E405 .00000000E 00 .00000000E 00 52 54.0480 MH 7016497402E405 .00000000E 00 .00000000E 00 53 54.0480 MH 7016496000E 00 .00000000E 00 .00000000E 00 53 54.5419 MH 7016436466E405 .00000000E 00 .00000000E 00 54 5.5158 MH 70164374666E405 .00000000E 00 .00000000E 00	14 54 9.2757 MH 7016248541E+05 .COCCOOCE 00 .COCCOCCE



																																						DATELISION												
00	000	000	200	000	000	00	00	00	00	00	00	000	20 4		000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00							1	7	0			2					
COCOE	DOCCE	10000	30000		0000	30000000	OCCCOCOE	BOCCE	3000000000	COCCOCCOE	OCOOOCCE	OGCOCOCOE		000000000000000000000000000000000000000	DOODE	DOOCE	COCCCCCC	COCOCOCCE	COCCOCCOCE	300000000	COCOCOOOE	COCCOCCOE	COCCOCOC	OGOGGGGGG	COGOOOGOE	300000000	000000000	00000000	COCCOCCC	SOCOCOCO	ODCOODOOF	OCCOCCOC	0000E					COMPACTED			<u> </u>	V 1 V			×			,		
	20000000	0000000	0000		0000000	0000	0000	.00000000	.0000	00000	00000	0000	0000000	0000	00000000	0000000	0000	0000	.0000	.0000	.0000	.0000	0000	-0000	.0000	.0000	0000	.0000	.0000	.0000	.0000	.0000	.00000000					2			FUNCTION	NOT TONIS			FUNCT ICN					
(cont.)	0 0	000	2 6	000		00	00	00	00	00	00	000	200	200	00	00	00	0.0	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00					3336 CELLS		l	2	ū	•		T.					
9 Ш	1	u 4	u u					ш		ш	ш							ı	ш					II.	.UII				i			211			8	i i		3336		7	1	7 67	2		2					
CUUUUU	00000000	00000	00000	10000000	90000000	20000000	00000000	00000000	COOCCOOCE	COCCOOCE	00000000	20000000		00000000	40000000	000000000	20000000	00000000	00000000	300000000	00000000	300000000	COCCOCC	COCCOOO	COCCOCOC	300000000	00000000	00000000	30000000	OCCOCCCE	COCCOCCC	300000000	COCCOCCE		£P			111111		CN TS	ENT	ENT IN	CN IS		ENT					
		•	•				5							•			2	5	5			7	5	ľ	•	•		. 5	5	•					25			STATIONS.	3	FUNCTION	SEGMEN	ONC. LCN	FUNCTION	148	SEGMENT					
01E+0	336+0	835+0	. 0	55F+05	3 7	6F#	#	H	267E+05	80E+0	7 E	694E+C	106106	536407	195405	063F+05	887E+05	745+0	765+0	622E+05	788E+05	33E+07	75E+05	504E+05	727E+05	\$0+356¢	42E+05	846E+05	399E+0	678E+05	110E+05	386+07	991E+05		*	1	S;	E (W)		#	RE IN	NI UO	1	Ш,	ARE IN					
159202	58447	59.97	200	56761	57499	95244	55791	156616	51452	154856	25706	56556	166776	6115514	- 152813	53720	-154598	51545	152545	150926			149691				149696	150628				.643738	36		CDA7* G		TERS	ONS.			11	· ·	1		62 A					
1	-	•	•			,		-	-	-	-	-	•	•	-		-		-	Ī	-	9.	-	-	•	-	-	-	-	ï	7	•	146		5		ARAME	RVAT							L					
70	0	0 0	2 0	00	0 0	0 (1	0	0	0	0,	0	0 1	Þ.) ¢	0	00	0	0,	7.0	7.0	2	0	20	7.0	70	0	0	70	70	7.0	76	0	0		*		5)1C	SAAR DRYFRVATIONS.	a	ON I	SEGME	NO NO	THE IN		SEGMENT					
		80		MH								BH					ВН		. ge				MH					ВН						(*) O31	*		ITERATIONS (MAXIMUM), (1) IC PARAMETER			FUNC	CAME FROM SEGMENT	TO SCI	THE PRINCES OF	*	FROM					
07	41	1.5	0 4 4	40	4	70	45	45	6.5	45	45	45	400	118	4.3	, 60	63	83	83	22	22	75	62	62	62	41	41	41	8960	99	6.0	7.4	040	CURRECTED		ı	MAXIM	ISTACK DREEBVATION TIMPS.	CD IN	000	CAME	010		CUTTO	CAME					
16.3007	19.68	19.68	9777 EC	27.20	27.20	27-56	30.96	30,9645	30.96	34.7245	34.72	34.72	34.42	21.9204	42.50	42.59	42.59	47.07	47.07	49.4822	49.48	50.12	53.80	53.80	53,8062	57.28	57.28	57.2841	89	0968	.8960	1.4074	4.80	TO BE C	RETA		ONS	TION	111					W EXE				101		
		64 9	6.5	107	67	67	49	64	64	64	64	64	64	* 4	60	64	16 49	64	64	64	64	64	64	49	64	64	64	4	4				6 50	RS TO	AL PHA DF! TA BFTA		ERATI	SERVA	FLOCKS					8661				L		
8 16	1111	80 0		1	0 0			8 16		8 14		8 16		0 10			8 14						8 14		8 16		7	-	-	8 16			8 1	AMETE	23.65		1	A DR	4					84°46					4	
7	1	- 1	-	1		7	7	7	1	7	7	1	- 1		-		7	7	1	1	7	1	7	-	•	1	7	7	7	-		-	7	PARAMETERS	*			18151						14.5					141	

	.16c060£-67 (14)	-01 (35)								
BASIC IMPUT CAND I	.150000E-GO .160000E-G7 .16EE	*2296000E+02319 .605600CE=01	.24639581E+C8 .60410640E-C2 .5015G392E+C2 .35686E3EE+C3 .23399700E+C3 .83661994E+O3	1 2	310 010	L62= .99400C0E+02 L63= .26800C0E+02 L64= -1996CCGE+02 L65= -252660C0E+02 L65= -16920C0E+02		RATIO OF COWELL STEP TO RUNGE KUTTA 4 RAXIPUPA6400E+02		00CIAL -55304203E-02 41624532400 *2663477F577 1300*67**
	.00 .492000E+04 .492000E+03	2296C00E+02219 .6056GCGE-C1301	.2311454CE+02	E=00 W/CDA = .351C0035E+01 IE+01 D2 =15684000E+02	-05 J4=1649CCCOE -06 J9=53CCOCCOE -25846DCDCE-07 -2219CCCCE-07 -16050CCCE-08		PERTURBATIONS	A= 1.000 .1562E-01	*	ONSTANTS GR FÅRTH GEGTUS - FE
	.*01 .360000E-00 ,750060E+00	SIGMA TABLE .2296 .2296	ALPHA= DELTA= BETA = A.2 = V =	CDA/W = .2849G00GE-00	-,3320000E-06 J8= -,3320000E-06 J8= 121= .000000000E 122= .15500000E+ 131= .4500000E+	142=-	USED FOR PLANETARY	TFFERENTIAL EQUATION SUBROUTINE GAUSS JACKSON TEP SIZE - INITIAL* TOROGE-01 TOROGE-02 TOROGE-03	USE N1 =10 N2= 6 FOR V HATRIX	CLECIMAL -4375269CE-02 32534026356G -49787546E401 7522112562G -1360849GE+04 5409474744
EMD	#BOUNDS .150000E+01 .150000E+01 .100000F-07	101 .2296000E+02119	X = .20394186E+08 Y = .81049750E+07 Z = .11063023E+08 XD01* -11454234E+05 YD01* .12760866E+05 ZD01* .14863762E+05	ATMOSPHERE - LOCKHEED	GM= .55304203E-02 J2= J6= .6460000E-06 J7= J21= .0000000E U J22= .1566400E-05 J31= .1728700E-05	. 13720000E . 13720000E . 41660000E . 93780000E	THE FOLLOWING BODIES ARE NONC FORMULATION	DIFFERENTIAL EQUATION SUBROUTINE CAUSS JACKSON STEP SIZE - INITIAL 100 NOT RECOMPUTE PERTURBATIONS	EQUATIONS OF MOTION USE NI VARIATIONAL EQUATIONS USE NI NO T MATRIX	DPEGA E ALPHA G FLUM

737510377420 223146314620 323146314620 314631463140 614643432460 3044672720	in the second se						
73751 22314 22314 31463 61464 3044							
.34439335E404 .34876230E+06 .34874234E404 .298374108E403 .12298530E 01 .10782109E-00	ICN 15 2	IGN 15			-		
.R. ELOCITY //E.R./MIN.	FUNCTION	FUNCTION FUNCTION	(cent.]				
N.M./E.R. 1-0, VEL F1/SEC// 1/EPS: (MOON) (MARS)	15 62	1 21	Pigure 27 (cont.)				
565605075320 452000000000 132071269100 444250714340 723146314620 355337552028 422335136140	2 ARE IN SEGRENT	62 ARE IN SEGMENT 2 NEW FUNCTION IS 1 ARE IN SEGMENT	43-12			W	
.23454865E+05 .20925738E+08 .321740£0£02 .10471976E+01 .33295130E+06 .81497900E+09	CAME FROM SEGMENT OLO FUNCTION 15	CAME FROM SEGMENT DLD FUNCTION 15 HTTON CAME FROM SEGMENT		9-1			
E.R./A.U. 1-O. DISTANCE G DEG/SEC/FRAD/MIN RELATIVE MASSISUNI (VENUS)	73	14.09.51 BEGIN EXECUTION CAME I OLD EI CAME I CAME I CAME I CAME I					

MIN. Figure 28. Computed Values	4675-87530 646.21816 4630-63175 591.17461 107.95173	107.90175 107.83470 1 FUNCTION IS 2 1S 2 FUNCTION IS 2 1S 2	13 FINCTION 19 2	1 FUNCTION IS 65 WITHIN THE CATA SP	887335839479E_C344C7574153	.17022679758151E-02 FUNCTION 1S 2 FUNCTION 1S 2	15 FUNCTION IS 2		
COMPUTED VALUES FOR ITERATION 1 7/ 8/67 885.000	TRUE ANH = 161,33899 APEGEE HT = 16001 - 3.00450 PERIGEE UDDI = 2.96157 PERIOD(K) =	.23399700E+03 .83661994E+03 .83661994E+03 .CAME FROM SEGMENT 12 ARE IN SEGMENT .OLD FUNCTION IS 2 NEW FUNCTION IS .CAME FROM SEGMENT 1 ARE IN SEGMENT .OLD FUNCTION IS 2 NEW FUNCTION IS	14.09.58 BEGIN EXECUTION: 14.10.02 BEGIN EXECUTION COMENT AS ARE IN SECHENT	13 ARE IN SEG	4E-C1 -+443600	7/ 8/67 982.07495 MH36221085592795E-01 .26694674863984E-07 -11809264324098E+0136221085592795E-01 .26694674863984E-07 CAME FRUM SEGMENT 21 ARE IN SEGMENT 13 2 CAME FRUM SEGMENT 13 ARE IN SEGMENT 62 0LD FUNCTION IS 2 NEW FUNCTION IS 2 14.11.38 BEGIN EXECUTION	14.11.40 BEGIN EXECUTION CAME FROM SEGMENT 62 ARE IN SEGMENT		

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	7-96	ul.	30000	104100	0	3	300	20	20000		22	\$145316.77	
	53601,2185	-	*0000E	(00(60)	000	(05)05	. 0000E	000	AGGGE GG		9 0	14832E-C	
	3400 06	**120E=02184	* 00000	1 3	30000	50	3 6	200	000000000000000000000000000000000000000		CCOF	145225-9	
	7	.4371F-0012P1	000	COLPDI	10000	5 =	20	200	0		CCEC	145334	
	-	0	0	CO(PC)	30000·	0	300 COE	00	CCCCE CC		CCOE 0	145338	
	3622.5	160-39655	033	194109	30000*	3	C	30	Ç		D 3000	145342.5	
	3623.5	94E+03	00	-	*0000E	-	00	00	COOCE CC		OCOE O	145342	
	53626.4341	*4828E-00(RO)	30000*	-	30000°	5	H 000		0		COE O	4434644	
	3630-2	1 7	30000	104103	3000	5 6	ш u	0 0) c		0 0000	145254.	
	53637.9419	4840600	0000	-	*	5 0	3 5	ے د			COFO	145357.9	
	53638 5792	56735+03121	000		-0000F	0	2 (2)	2,0	0		CCOE 0	145356.	
	364	511	.0000E	-	.0000E	0	0	10			CCOE O	1454 1.7	
	53645.5158	52396+001	*0000E	-	*0000E	100		00	Ç		0 3000	1454 5.	
	3649.2	4	-0000E	(04)00	*0000E	0	111	00			0 3000	1454 5.5	The second second second second second
	3650	0	*0000E	-	*0000E	0	111	00	0		COE O	145416.9	
	3653.0	02E+00	*0000E	CO(PD)	OCCCE.	-	.0000E	0	.0000E 00		COE	145413.0	
	35	100+100	- OCOCE	-	30000	4	#0000 #	2 9	3 4		CCOE	145416.6	
	53660,5955	. 5792E+001RD1	30000	001707	-00000	000	. 00000	000	20000			145427	
	•	REFFOOT	30000	* ***	- 0000E	-	4 11	60	3 Q		CCOE	145424.3	
		.6218E+00(RE)	.0000E	CO(PD)	.0000E	0	ш	0	OCCCE CC		CCCOE OC	145428.	
	3671.875	. 62 70E + 00 (RU)	.0000E	-	.0000E	-	.0000E	2,	0		CCOE	31.8	
li	10	5688E+031R1	30000°	4	30000-	-	1.84	30	9		3000	145434	
	53675.6353	E .	.0000E	Her h	.0000E	100100	LRI 6	25	0 4		900	8145435.64	
	53619,3952	.6740E+00(RD)	* 00000	COLPUI	*00000	lade I to	100000	2 6	occupie oc		00 -000	5443.	
	3685.5	5467E+03(R)	.0000E	I	.0000E	0	1 111	000	0		COE	145445.5	
	3686.9	.7016E+00(RD)	.0000E	9	.0000E	0	ш	00			COE O	145446.	
111	63690.6750	.7231E+00(RC)	-0000E	CO1001	. 0000E	9	J.	000		1	COE	145450	
			€0000€	4	-0000E	***	ш.	0 0			CCOE O	143434	
	53696,8583	-,5535E+83(R)	* 00000	00(A)	90000	00(11)	. dange	2 6	00000 00		00 50000	8145458-19	
	. 0	7748F+00(RD)	DOODE	0	OCCOP	-		00	ı w		CCOE	1455 1.	
	3705.	7923E+000	0000	-	00	(05)00	. ш	00	SOCE		CCOE	1455	
	53708-1381	5311E+03(R)	-0000E	-	30000	-		000	OCCE C		CCOE O	1455 B	
	13709.4747	*818184001851	*00000	00000	-0000	-	J 4	9 0	20000		00 30000	145612.7	
	53716.9946	*8565E+00(RD)	-0000E	*	. 0000E	00 (00)	300	0	3000		CCOE O	145516	
	19	5311E+03(R)	.0000E	-	.0000E	-	300	00	OCCE C		CCOE 0	145519	
	154	.8807E+00(RD)	.0000E	~ `	.0000E	0	000	000	OCCE O		000	145520	
	53124.5145	42525 +001801	10000	000	* 0000E	00 (00)	00000	200			CCOE	1455	
	.885	\$280E+031R)	.0000E		0000	-	300	0	0 3000		0 3000	145530.8	
	32.0	. 9530E+001RD)	30000€	o	30000°	0	300	30	0	1	CCOE 0	145532	1
	3735.7	9685E+0013	00	~ ~	5 6	6	000	200	o c		0 4000	145555.1	
	537.59.5543	- 5180F+031R1	- 0000E	00 43	2 2	00(6)	U U	000	0		OE O	145542	
	53743.3142	.10366+01(80)	. 0000E		.0000E	010	300	00	0		CCOE 0	145543+3	
	53747.0742	10516+014	30000°	00(PD)	*0000E	0	300	00			CCOE O	145547.	
	3750.	*1076E*014	*0000E	-104 HOD	-0000E	4	300	000	Φ 9		CCOE	14555C+E	
	53753.6334	4995E+05(K)	• 0000	0000	00000	0 0	300	200	20000		0 10	145554	
- 1	3758.35	1315+0113	30000°		30000°	-	305	00	3000		CCOE 0	145556.	The state of the s
		+014	30000°	(Od)00	* 0000E	3	300	36	00		CCOE @	1456 2.	
	53764.9133	4823£+03{R]	30000°	00(A)	.0000£	-	W 10	000	00000		• 0000E 00	81456 4.41	
1	3765.8	-	30000		5 4	100	U U	200	3 5		COF	1456 9-6	
	53773,3938	168	.0000E		00	50	SOF	0	CCCCE OC		COE O	145613.	
	3776-193	4780E+031R	-0000E		000	OLE	63	00	00		CCOE O	8145616-19	
					Tinne	29.	Residual Output						

•						
147						
TYPE						
RMS RES/SIG		Sumary				
z 10 10	(21)	30. 1068				
TYPE	(R)	Pigure				
RMS 5/5/1G 35/8E+03 1393E+02	.8186E+03 .6806E+02 .8868E+03 .7103E+02					1
63 63 139	26 .26 .11					
TYPE N (RD) 63	(RC) (1					
NOT THE REAL PROPERTY.	1E+01 (3E+02 TE+0E t					
RMS RMS/51G - 161216E+01 - 266209E+02	.196791E+01 .324953E+02 .202287E+01 .334027E+02					
AT N 206	116					
STAT	08					

	v *23765255E+05		*21986359E-01 (28)	.49200000E+03 (29)	.2376522EE+05 (31)	a		, 160%c222E-00 (34)	
ITERATION 1 (22) Sec. DAIA POINTS MERE USED IN THE SOLUTION . (23) CHRENT SOLUTION IS BEST SO FAR (24) CURRENT SOLUTION IS	### CDA/W G	CONTINUE SOLUTION FOCTAL MACHINE UNITS 766361054213543440	#### RMS# .27708293E+02 FOR THIS SOLUTION (27) CORRECTIONS .2520716FE-0248463704E-0485928347E-04 .49035265E-03 .60568054E+0209348143E-01 .4623789E-0847309442E-094770954E-09	.150000006.03300000006.001000000001.	NETTING BOUNDS (30) NEED SOLUTION IS .26515112C+02 .89689684E+02 .45733610E+02 .24780897E+08 .24780897E+08 .24780897E+08 .2478984E+02 .2548471E-05		****** PREDICTED RHS* . D0560426E+00 FOR NEXT SOLUTION (33)	A BRIA DELTA BELIA A R. 1.10672878896-62 .75775623E-03 .10672877E-02 .23999429E-03	7

CORRELATION MATRIX

		(33)		(90)							H
10		1,000		GM 99958E+14 99958E+14 80274E+13 26412E+10 17923E+13	485E+19			64625260 50545640 57522760 65601210 42744250	24.10		
6		200.1		W. W. W. W. C. C.	0*	1		56055C4264 5006437550 4202527657 2366424765 2102734374 1103454	(63)		
6 0		1.000		CDA/N 2,489418E 2,457622E 2,2657622E 2,119993E 2,139993E 4,149645E				560730017 212620251 437646770 368717212 471551615 0156131615			
1		1.000		838E+06 087E+C7 339E+67 066E+07- 445E+67-				7421752462015 5640251246025 5506566147054 5606566147054 5010642016074	·	·	
90		1.000 -130 -130 -155		E+05 9.81 E+05 2.93 E+05 5.81 E+03-1.01 E+01 1.00				131073 701047 113053 605664 154053		re 31 (cont.	
2		1.000 .76/ 116 .944 .295	Ŧ	R 0-3-116567 0-5-184874 0-9-916563 1-226783				0577254063 0505510251 0673155662 0220147135 101465103		7.1gure	
4	1.000	.354 .577 .332 .455		A 163661E+C 553297E+1 969401E+1 293515E+1				31320365 07621401 05345020 16225640			
3	1.000	.143 400 773 .041 .953	25	BETA 6.797189E+10-9.16 13.844057E+10-1-55 1.214932E+11 1.96		1		_41626231722070306030463604457 641372030452036221042373405456 43470466034603255 7525			
2	1.000		= .49796E-25	TA 4E+10 6.79 5E+10 3.84 1.21	96+10	76+11 56+12 86+11 56+07 56+10 86+07 66+16	0E+14 9E+14 1S1	1722070306 0452036221 4347 <u>0</u>	07030 01610 63420 13740	20510 41010 67120 11700 35500	
1	-,900	. 574 . 502 . 100 . 521 . 251	O	DELTA 10 7.162304E+10 6.462455E+10	J3 12-3-66351	12-4.510847E+11 13-8.4128E+11 15-6.47128E+11 17-3.451625E+07 10-2.906415E+10 17-3.313188E+10 17-8.312186E+16	14 1.272090E+14 1.223409E+14 JUTPUT UNITS1	66137203	020225015 053723533 0010664323	25200463102033446720 3614735230336320544 56532047206466046567 13415427407234565631 44436266004233643035 1331061516	
	- N.M.+	5 9 8 6 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SCATTER COEFFICIENT ATA AT .101008	ALPHA 8.739871E+10 7 6	J2 -1.047626E+1	-1.0125446+12-4.5108476+11 -6.702075E+11 1.391875E+12 3.218844+11 6.467128+11 -3.448647E+07-3.051625E+07 -4.08642E+10-2.906415E+10 7.430841E+07 5.313188E+07 1.081604E+17 8.312186E+16	1.788363E+14 1.272090E+1. 1.223409E+1 ATA (OCTAL OUTPUT UNITS)	2747006111000	33117632523102022501507030 2526764033105372353301610 33653013226301066432363420 41772105531403761714213740	61425200463102033446720510 42136147372303363205441010 33156533041205466046567120 152134156274073436554311700 64444436266004233643035500	ATA INVERSE

(37)						
.590916F-62 .355247F+C0 4.182627F+03 .791861F-CE-1.9260695-06 1.6322C9E-14 .703271F-C7-1.9867918-03 1.1838928-12 .326400E-06 1.6126948-03-6.072769E-13			26563320520365752550 3366334050604310335007343662600120 4151766032750550556510 5670517052205006522076760 127603201235003307460334264160304014736345304304126147523960 127603201235003307460334264160304014736345304304126127420 0253532026500C6410670657672651704010277511437406724C31762210		1.60966-01 6.46738+01 1.27768-01	FUNCTION IS 0
2,583372E-06 1,36553E-01 5,759726E+04 1,493846E-04 2,963530E+01 2 3,96745E-02-1,793855E+03 1 9,345449E-11 2,894611E-05 1 3,183901E-08 2,461613E-03-8 2,646730E-08-1,300181E-03 1		6500 04.057745315234C0	666024132265633205203657525560 4450407723464344050664310335007343662640124 4716 50354151766032175657055510 567051705220500685224767660 5060215901276032012350033074603342661603040147363430430 570072797537217103012731324220 3307462544194666071764350		1.6073E-03 2.39996+02	15 ARE IN SEGMENT 62 2 NEW FUNCTION IS 0 62 ARE IN SEGMENT 63
1.091271E-06 -1.002007E-06 1.135765E-06 -1.425805E-07-1.474110E-07 -4.203502E-07-1.474110E-07 -4.203502E-01-1.474110E-07 -4.203502E-01-1.4540233EE-02.2.4540643E-07 -8.433955E-03-1.003945E-02-3.786042E-02 -8.433955E-03-1.003945E-02-3.786042E-02 -9.441134E-10-1.8949656E-11 -9.44214134E-09-7.329911E-09-2.613024E-08-3.18	1,210931E-09 -9.307211E-10 7.812334E-10 ATA INVERSE (OCTAL OUTPUT UNITS)	7627324041360 4544636257330 463402605700 156771211000 0244261275702261253516500 440034522176140743724706445744346504	66110541016201433570335230334357127666024132 73501225650404723544535170_3174724435460772 2081473764740440220253533341664534710_5035 10675665034402461437125503246031302596021509 31033011737002450276345470_27347207570007779 376634002433030123775345302671472757750_0446	5656504342260 5531014607170632364477460	SQUARE RD01 DF DIAGONAL OF INVERSE 1.0446E-03 1.0657E-03 7.5776E-04 3.4798E-05 2.7951E-05	CAME FROM SEGMENT OLC FUNCTION IS CAME FROM SEGMENT

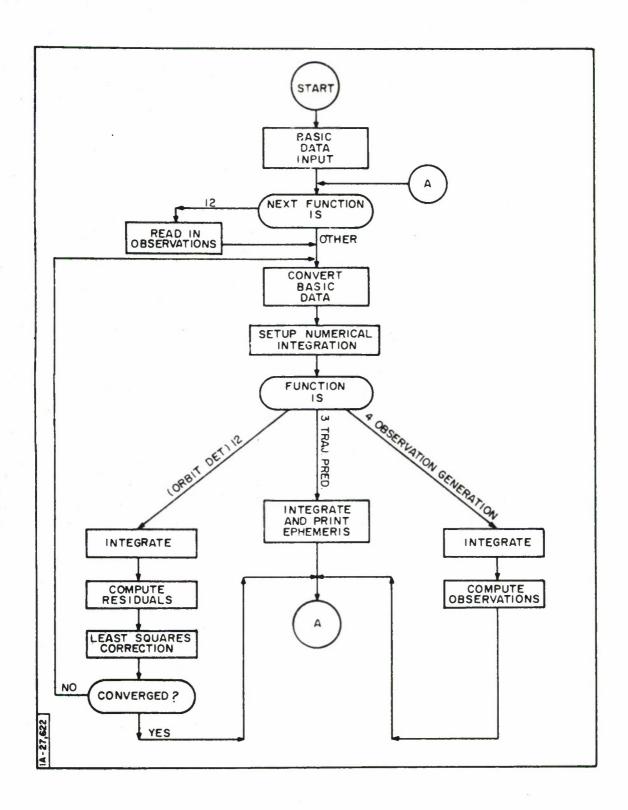


Figure 32. General TRACE-D Flow Chart

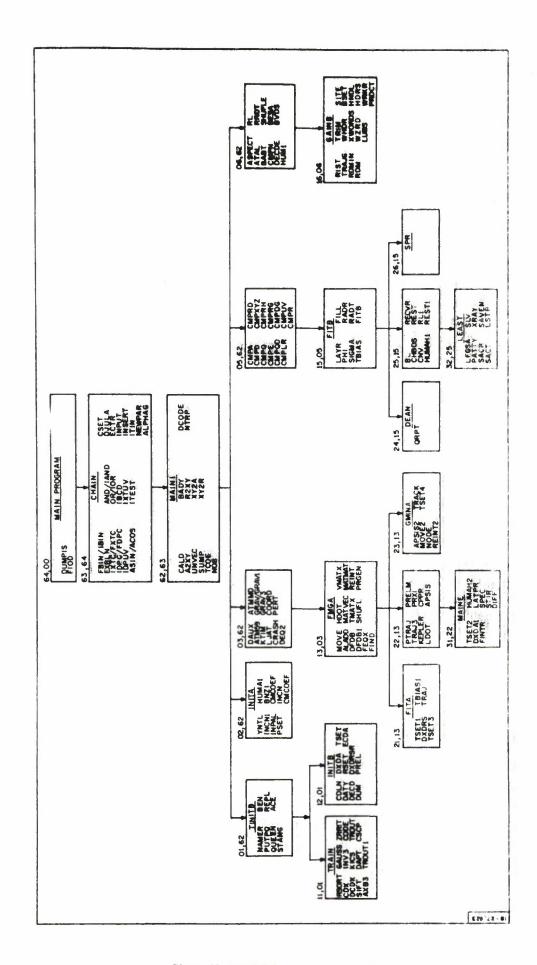


Figure 33. TRACE-D Segmentation Flow Chart

Section 5.

Programming Information

5.1 Structures and Flowcharts

Figures 32 and 33 are both flowcharts of the TRACE-D program; however, each is geared to a different level of description. Figure 32 depicts program paths determined by the function to be performed with only basic operations considered, while Figure 33 presents pertinent programming details also.

Since the TRACE-D program is extremely large (approximately 22,000 source language cards) and can not be fully contained in core, the segmentation mode of operation is employed whereby the program becomes several coreloads. Figure 33 shows the levels of segmentation employed and the makeup of each and every segment. The fact that only the segments along a single vertical path are in core at any one point in time solves the storage program.

The number appearing outside each segment block in Figure 33 serves to identify its level and position in the structure. Those subroutine names underlined are the control programs, which among other things, transfer control to the proper segments for each major function.

5.2 Tape Usage

The TRACE-D program employs many tapes to handle input-output data as well as intermediate calculations. The tape requirements for each option consists of a basic set common to all functions (listed in Table 11) plus a unique option-dependent set. All of the possible option-dependent tapes are listed in Tables 12, 13, 14 and those that are mandatory are appropriately marked. Please note that no more than five tapes from Table 14 may be used in one run (in addition to the basic set, of course).

The above description has been included for completeness; however, as previously mentioned, the user may obtain a running deck for any option he wishes to choose which will set up all appropriate tapes for him.

Table 11.
Basic Set of Tapes

TAPE NUMBER	NAME	FUNCTION
	LIB1	Program tape #1
	LIB2	Program tape #2
2		System Input Tape
3		System Output Tape
4	PTAPE*	Necessary Scratch Tape
3		Necessary Scratch Tape

^{*} This is a necessary input quantity for all runs.

Table 12.
Trajectory Prediction Tapes

TAPE NUMBER	NAME	FUNCTION
7	CTAPE	Planetary Coordinate Tape
17	NTAPE	Binary trajectory tape (nominal) for trajectory differencing (program generated).
19	DTAPE	Binary difference tape for trajectory dif- ferencing.
15		A binary trajectory tape generated by the program and saved.

Table 13.
Observation Generation Tapes

TAPE NUMBER	NAME	FUNCTION
11	ETAPE	BCD tape of observations program generated.
7	CTAPE	Planetary tape
10	IFLAG(16)*	Scratch tape (for trajectory)

^{*} Necessary tape for this option.

Table 14.
Orbit Determination Tapes

TAPE NUMBER	NAME	FUNCTION
11	IBCDI	BCD tape of observations
12	IBINI	Binary tape of compacted observations
7	CTAPE	Planetary coordinate tape
9*		Scratch tape (for normal matrix)
5*		Necessary scratch tape
10*		Scratch tape (trajectory)

^{*} Necessary tapes for this option

5.3 Subroutines

This section is devoted to a complete listing of every subroutine in TRACE-D with a functional description and other pertinent facts also given. In some cases two or more routines are identical in function and differ only slightly in name. This is due to the segmentation rule that the same routine name cannot appear in more than one logical path (i.e., one complete coreload). Therefore, since some routines were needed in more than one path only the names were changed not the content. The routines are listed alphabetically in Table 15 and the information given is self-explanatory.

Table 15. Subroutine Listing

	ROUTINE SIZE	312	1212	141	133	14	503
	FUNCTION	Converts orbital elements to car-	Sets up the code lists for all	radar parameters Adds longitude independent terms to the variation-	al equations for alpha Computes right ascension at Greenwich at 0 hours of	given Julian date Logical "AND" func- tion for two	variables Interpolates for and prints lati- tude, longitude and altitude when BETA = 90°
	CALLS SUBROUTINES	BADY	OUEEN				CALD, NTRP, SHUFL
	CALLED BY SUBROUTINES	INCN, INCN1, KICS, ISET	TRAIN DUM	TRACK, TRAJ, TRAJ3,			TRAJ, TRAJ3
216	ZEGPHP	×		×	×	×	
e e	- K K L P K E	×		×	×	×	×
ns	O	×	×	×	×	×	×
	SEGMENT NUMBER	62	01	13	63	63	22
-	NAME	A2XY	ACE	ALADD	ALPHAG	AND	APSIS

Table 15 (cont.)

	ROUTINE SIZE				422	141	471		116		543		115				205			241			1000		401		111	
	FUNCTION				Same as APSIS	Computes arcsine	and arccosine	compares aspece	angles Finds I, J ele-	ments of matrix	Computes atmos-	pheric density	Channels density	evaluation to	appropriate	routine	Solves the system	AX=B using Cramer's	Rule	Computes BABT where	B and A appropri-	ate matrices	Computes solution of	two-body problem	Performs data	coding	Finds I, J element	of matrix in spe-
	CALLS SUBROUTINES				NTRP		90755	VIC					ATM59,	LJAT														-
	CALLED BY SUBROUTINES				TRACK	PTRAJ	E 6	SILE	BABT		ATMMD,	LJAT	PERT				INV3			SITE			A2XY		NAMER		REST,	RESTI
NIO	A H	4 C	pы	z	×			×	×		×		×															_
	N A	o 6	٠ ×	ম		×					×		×															-
US	N R	ОР	4 [×		×				×								×		×	_
	SEGMENT				23	63	. (co.	0.5		03		03				11			90			62		01		25	
	NAME				APSIS2	ASIN/	ACOS	ASPECT	ATAL		ATM59		ATMMD				A XB 3			BABT			BADY		BEN		BL	

Table 15 (cont.)

	ROUTINE SIZE		251	37.1	1	203		216			210		100		209					120		1031		_
	FUNCTION		Converts and prints	bounds and sigmas	and labels	Builds variable	data formats	Computes complete	date Irom Julian	date	Computes data loca-	tion from BCD name	Packs data into one	word	Control program for	segment 63				Modifies bounds for	orbit determination	Computes coefficients	location constraints	
	CALLS					IDPC,	AND				IXTUV.	LTIN	IDPUV		INPUT,	CSET,	DJULA,	ALFRAG	ITIN ITIN					_
	CALLED BY SUBROUTINES		INCN	IUNH	TIMOR	HNDL		INITB, HNDL,		RADT, TRAJ,	DUM		RSORT		MAINI	_				LEAST		INITA		_
NI	C A T A	шz		;	<	×					×				×									
USED	RAPH	저 표									×				×									
SIO	民田口田	H	×								×		×		×					×		×		_
	SEGMENT		02	91	70	90		62			12	1	11		63					25		02		
•	NAME		BNZI	£	DSEI	BVDS		CALD			CDLN		CDX		CHAIN					CHBDS		CMCOEF		_

Table 15 (cont.)

	ROUTINE SIZE	456	623	ì	364		626		451		136	925		200		530	None on d
	FUNCTION	Computes azimuth	partials and rest- dual Computes topocen- tric declination	partials and residual	Computes geocentric	tials and residuals		partials and residuals	Computes little	residuals and partials	Computes noise		partials and residuals	(I)	duals	Computes range par- partials and resi-	
	CALLS SUBROUTINES	PHI					PHI,	CMPR				CMPR,	FILL	CMPRD,	177		
	CALLED BY SUBROUTINES	RADR	RADR		RADR		RADR		RADR		SITE	SITE		SITE		SITE	
NIC	ч н ч о н	z									×						
USED																	
plo	民国口出口	×	×		×		×		×			×		×		×	
	SEGMENT	90	90		05		05		05		90	90		0.5		50	
•	NAME	CMPA	СМРА		CMPDG		CMPE		CMPLR		CMPN	CMPQ		СМРОД		CMPR	

Table 15 (cont.)

	ROUTINE SIZE	734	340		989		```	909		514			144			142		909		143		
	FUNCTIONS	Computes range rate partials and resi-		sion partials and residuals	Computes topocentric	RA, HA partials and	residuals	Computes U, V par-	tials and residuals	Computes X, Y, Z	partials and resi-	duals	Checks for conver-	gence in orbit de-	termination mode	Packs data into	one word	Reads JPL tape and	performs interpo-	lation Controls output	during trajectory	prediction
	CALLS SUBROUTINES	РНІ														IDPUV				rate of the state	PRELM, PTRAJ	
	CALLED BY SUBROUTINES	SITE	SITE		SITE			SITE		SITE			LEAST			CSCP		PERT		4 1 2	CONT	
N O	NEGATA																	×				
	RAPHRE			-			-	_					_		-			×			×	
USED	REDBH	×	×		×			×		×			×	-		×		×				
	SEGMENT NUMBER	0.5	90		05			05		05			25			11		03		(77	
•	NAME	CMPRD	CMPRG		CMPRH			CMPUV		CMPXYZ			CNV			CODE		COORD			CFFR	

Table 15 (cont.)

	ROUTINE SIZE		447			1174			135	217		276				270					107			141		e) m m1	
	FUNCTIONS		Tests for vehi-	hicle below critical alti-	tude	Compacts and	codes data	Sets up some	constants	Prints deleted	observations	Prints data	types used in	partial genera-	tion	Computes deriva-	tives for equa-	tions of motion	and variational	equations	Decodes a data	word coded by	CDX	Decodes words	coded by CODE	Decodes packed	data word
	CALLS SUBROUTINES		NTRP,	HDOT			REPL, IDPC			TCDE		DECD				MOVE, PERT,	MATVEC,	GRAV2			IXIUV			VUIXI		IXIUV	
	CALLED BY SUBROUTINES		TRACK,	TRAJ, TRAJ3		TRAIN		CHAIN,	TSET	SIFT		MUG									CSCP,	RSORI,	TROUT	KICS,	SUMP	DATY	
NO	Q P T A	ыz	×					×				×				×								M		×	-
SED	R A J F	ЖШ	×					×				×			_	×		_						×			-
US 0	жырн	H	×			×		×		×		×	_			×	_		_					×			
	SEGMENT NU NUMBER		03			11		63		11		12				03					11			62		90	
	NAME		CRASH			CSCP		CSET		DAPT		DATY				DAUX					DCDX			DCODE		DECDE	

Table 15 (cont.)

	ROUTINE SIZE	133	273	1472	376		6	723	177	//1		1045		355		355	342	
	FUNCTIONS	Same as DECDE	Keeps simulation list current	Performs inte-	Computes non-	homogeneous terms for vari-	ational equations	Same as DFDB	1000	date	מסרט	Reads station data and stores it		Computes partials of pos and vel wrt	orbital elements	Same as DXDA1	Computes partials	of pos and vel wrt spherical coordi- nates
	CALLS SUBROUTINES	IXTUV	PRDCT	DAUX	NOB, DFDE1	MATVEC		CT ANTILL	nomanz			ACE, DATY, ITEST, REPL,	PUTPO					
	CALLED BY SUBROUTINES	SITE, HDRS	GAINB	TRAJ, TSFT	PERT			DFDB	TROTTE	CHATN	INCN, INCN,	INITB		TRAJ3		TSET	TSET	•
N Q <	Z E C P H P	×	×	×					1	×	2002AL 27 ALL 2011	×						
USED O T	4 4 7 6 8 8	×		×	×			×	×	×		×		×		×		_
US 0	REDBF	×		×	×		_	×	×	×		×				×	×	-
	SEGMENT NUMBER	12	90	03	13			13	31	63		12		31		12	12	
	NAME	DECD	DESA	DEQ2	DFDB			DFDB1	DIFF	DJULA		MUQ		DXDA1		DXDA	DXDRSR	-

Table 15 (cont.)

	ROUTINE SIZE	342	155	253	123	305	Ċ	35	183	c c	533			242		360		14000			1472		663	500	202	1
	FUNCTION	Same as DXDRSR	Codes an array	Codes an array	Extract routine	Conversion rou-	tine	Deposit routine	Generates a	matrix	Fills a list for	partials compu-	tation	Performs linear	interpolation	Used to end a	trajectory run	Sets up appropri-	ate magnetic	tapes	Control routine	for segment 21		Control routine	for sepment 13	for segment 13
	CALLS SUBROUTINES		IDPU, IXTC	ITEST							IXTUV,	UTRD									ISET1, ITIN	TSET3, TRAJ	TBIAS1	NTRP, LEAST		FITA, GAINA I
	CALLED BY SUBROUTINES	TSET3	DUM	CHAIN, INCN1	INPUT	INPUT		INPUT			RADR, CMPQ	CMPQD		PERT		MAINE					FMGA			MAINI		MAINI.
N O	NEGPHA		×	×	×	×		×						×				×								×
	医 皮 u u u u u u u		×	×	×	×		×						×		×		×								×
US 0	ж в О н н к в о н к н	×	×	×	×	×		×	×		×			×				×			×			×		×
	SEGMENT NUMBER	21	12	63	63	63		63	13		15			13		31		79			21	i		1.5	1	13
,	NAME	DXDRS	ECDA	ECTR	EXBLN	FBIN		FDPC	FEQX		FILL			FIND		FINTR		FIOD			FITA			TTTB	7777	FMGA

Table 15 (cont.)

	ROUTINE SIZE	35	1266	320		652			470				301			410			1351		
	FUNCTION	Extract charac-	ter routine Control routine	for segment 23 Control routine	for segment 06	Determines el-	liptic elements	given 2 points	Computes accel-	eration compon-	ents due to geo-	potential ::	Computes H and H	for minimum and	interpolation	Sets up page	headers for ob-	servations	Controls observa-	tion output	
	CALLS SUBROUTINES		TRACK	RIST. SITE.	TRAJG, HNDĽ, WZRP, DESA, ITIN											DECDE				CALD, HDRS, WHDR	
	CALLED BY SUBROUTINES	INPUT	FMGA	MAINI		KICS			DAUX,	PERT,	TSET2,	TSET4	CRASH,	SITR		HNDL			GAING,	TRAJG	
NIO	4 H 4 G E Z	×	×	×	1					×			×			×			×		
SED	247222	×								×			×								_
SNO	民国口田工	×				×				×			×					_			_
	SEGMENT NUMBER	63	23	90	}	11				13			13			16			16		
	NAME	FXTC	GAINA	CATNR		GAUSS			GRAV	GRAV1	GRAV3		HDOT			HDRS			HNDL		

Table 15 (cont.)

					1 2 3 4	ייייי די יייייי		
		ns	ED					
		0 %	HK	D A				
NAME	SEGMENT	М	A	₽	CALLED BY	CALLS	NOTTONIE	POTTAINT STOR
	NUMBER	Оын	О Ш Е Р В В В В В В	A O H Z	SUBROUTINES	SUBROUTINES		40110 ON
HUM1	90			×	SITE		Input-output	474
							conversion	
HUMA1	02	×	×	×	BNZI		Input-output	474
							conversion	
HUMAH1	25	×			XRAY, LSTP		Input-output	474
							conversion	
HUMAH2	31		×		DIFF, PRXI		Input-output	327
							conversion	
1AND	63	×	×	×	INPUT		Logical and	
							function	
1BCD	63	×	×	×	INPUT		Conversion	
							routine	
IBIN	63	×	×	×	INPUT		Conversion	
							routine	
IDPC	63	×	×	×	INPUT		Conversion	
							routine	
IDPUV	63	×	×	×	INPUT		Deposit	
							routines	
INCN	02	×	×	×	INITA	BNZI, R2XY,	Initializes	997
			4.75			XYZR, NOB,	input	
						INPUT,		
						A2XY,		
						ALPHAG		
INCNI	0.2	×	×	×	INCN	NEWPAR,	Initializes	1245
						NOB, ECTR,	input	
-		_			_	INPAL,		
						XY2R, YNTL,		

Table 15 (cont.)

SEGMENT B			SU.	USED IN	IN				
NUMBER D A 1 CALLED BY			0 %	H K	DAI				
T R E NAIN1 INCN Control routine for segment 02 12 x x x INITB DUM, TCDE, Control routine CALD, PREL, for segment 12 REST, NAMER CHACKS for incorrect input rect input stores all input stores and stores all input stores all in		SEGMENT NUMBER	M D E	A D d	4 & Q	CALLED BY SUBROUTINES	CALLS SUBROUTINES	FUNCTION	ROUTINE SIZE
O2			H	瓦瓦	шΖ				
12		02	×	×	×	MAIN1	INCN	Control routine	525
CALD, PREL, for segment 12	INITB	12	×	×	×	INITB	DUM, TCDE,	for segment 02 Control routine	360
02							CALD, PREL, REST, NAMER	for segment 12	
63	INPAL	02	×	×	×	INITA		Checks for incor-	261
FBIN stores all in- put Inserts character information words 11	INPUT	63	×	×	×	CHAIN		rect input	1662
Inserts character information words 11					J			stores all in-	
Figure Figure The continuation The continua								put	
11 x x x TROUT1 AXB3 Computes noise 63 x x x INPUT Computes noise 63 x x x x INPUT Tests for certain 63 x x x x CHAIN Checks the next function code in 11 11 11 11 11 11 11 11 11 11 11 11 11	INSERT	63	×	×	×	INPUT	INPUV	Inserts charac-	102
11 x x x x TROUT1 AXB3 Computes noise 63 x x x x INPUT Logical function 63 x x x x INPUT CHAIN 63 x x x x CHAIN 63 x x x x INPUT Checks the next function code in list and sets indicator 63 x x x x INPUT Extract routine for characters 63 x x x x INPUT Extract routine for characters 63 x x x x INPUT Extract routine 63 x x x x x INPUT Extract routine 63 x x x x x INPUT Extract routine 63 x x x x x INPUT Extract routine 64 x x x x x INPUT Extract routine 65 x x x x x INPUT Extract routine 65 x x x x x INPUT Extract routine 66 x x x x x INPUT Extract routine 67 x x x x x INPUT Extract routine								ter information	
11 x x x TROUT1 AXB3 Computes noise 63 x x x INPUT Character function 63 x x x X INPUT Character config- urations Checks the next function code in list and sets indicator Extract routine for characters 63 x x x INPUT Extract routine 63 x x x INPUT Extract routine 63 x x x X INPUT Extract routine 63 x x x X INPUT Extract routine 63 x x x X INPUT Extract routine 64 x x x X INPUT Extract routine 65 x x x X INPUT Extract routine 66 x x x x X INPUT Extract routine 67 x x x X X INPUT Extract routine 68 x x x X X INPUT Extract routine 69 x x x X X INPUT Extract routine								words	
63 x x x INPUT Logical function 63 x x x x INPUT Tests for certain character config- urations Checks the next function code in 11st and sets indicator Extract routine for characters 63 x x x x INPUT Extract routine Characters Extract routine Solves Keplers		11	×	×	×	TROUT1	AXB3	Computes noise	108
63 x x x INPUT Character config- urations Checks the next function code in list and sets indicator 63 x x x x INPUT Extract routine for characters 63 x x x x INPUT Extract routine for characters 63 x x x x INPUT Extract routine Solves Keplers		63	×	×	×	INPUT		Logical function	
63 x x x CHAIN checks the next function code in list and sets indicator characters confile for characters char	ITEST	63	×	×	×	INPUT		Tests for certain	117
63 x x x CHAIN Checks the next function code in list and sets indicator 63 x x x INPUT Extract routine for characters 83 x x x INPUT Extract routine 84 22 x x x INPUT Solves Keplers								character config-	
63 x x x INPUT Extract routine for characters 63 x x x x INPUT Extract routine for characters 63 x x x x INPUT Extract routine for characters 63 x x x x INPUT Extract routine Solves Keplers		7	;	;	;	NIVID		urations	106
63 x x x INPUT Extract routine for characters 63 x x x INPUT Extract routine 63 x x x INPUT Extract routine 822 x x TRAJ3		3	4	4	4	NT UTION		function code in	001
63 x x x INPUT Extract routine for characters 63 x x x x INPUT Extract routine 83 x x x INPUT Extract routine 84 22 x x x INPUT Extract routine 85 22 x x x INPUT Extract routine								a to a	
63 x x x INPUT characters 63 x x x INPUT Extract routine for characters 8								indicator	
63 x x x INPUT Extract routine R 22 x x TRAJ3		63	×	×	×	INPUT		Extract routine for	
R 22 x x x INPUT Extract routine Solves Keplers								characters	
I STATE I TRANS I COMMINISTRATION I STATE I IXI # 77 I	IXTUV	63	×	×	×	INPUT		Extract routine	091
	~	77	_	×	_	I KAUS	_	STATUS SANTOC	700

Table 15 (cont.)

	ROUTINE SIZE	505					4	163		578				1355			564		
	FUNCTION	Computes initial conditions from 2 R. A. E sets	Tests for orbit	adjusts times Latitude print	routine Accumulates ATA	matrix and re-	siduals	Computes longi-	tude and rate of longitude	Control routine	tor segment 32			Solves AX=E in	least squares	sense	Compute density	for Lockheed	Jacchia
	CALLS SUBROUTINES	SUMP, A2XY, DCODE, GAUSS, STRANG		NTRP, LDOT						SAVEN, SLV,	LSTP. RECVR, TCDE, ITIN,	SIGMA, SACR,	CNV				ATM59		
	CALLED BY SUBROUTINES	TRAIN	TRACK, TRAJ TRAJ3	STIR	RADR			LATPR		FITB				SLV			ATMMD		_
IN	A H A B H A		×														×		
	847051		×	×	1804			×									×		_
US 0	хвОпн	×	×		×					×				×			×		
	SEGMENT NUMBER	11	03	31	15			22		32				32			03		
,	NAME	KICS	KTIM	LATPR	LAYR			LDOT		LEAST				LEGSA		77.6	LJAT		-

Table 15 (cont.)

	ROUTINE SIZE	1125	155		516	,	1322	,	114	111		267			236	230		561
	FUNCTION	Controls output	for least squares Checks data gener-	ation indicators	Control routine for segment 62		Control routine for segment 32		Computes AB+C	Computes matrix	times vector	product Moves data from one	array to another		Same as MOVE	Finds list of names	for output	Decodes parameter list
	CALLS SUBROUTINES	HUMAH1			INITA, FITB, TINITB,	FMGA,	ITIN, FINTR SPEC, TSET2	TRAJ3										INSERT
	CALLED BY SUBROUTINES	LEAST	T. L.		MAIN Prog		FMGA		DAUX, DFDB	REINT	REINT2	DAIIY TRAI	TRAJ3,	TSET2	TRACK,	ISEI4 TRAIN,	INITB	CHAIN, INCN1
NI	A H A D H Z		×	:	×				×	×			<		×	×		×
	医女子中民田				×		×		×	>						×		×
SIO	ж в О в н к в о в н	×			×			_	×	>		;	¢			×		×
	SEGMENT NUMBER	32	16) 1	62		31		13	13)	c -	C I		23	01		63
-	NAME	LSTP	TIIRG		MAINI		MAINE	•••	MATMAT	MATURC		110%	TA OLI		MOVE2	NAMER		NEWPAR

Table 15 (cont.)

ROUTINE SIZE	141	252	371	1231	641	126	571	427 345
FUNCTION	Finds correct geo- potential coeffi- cient	Interpolates for nodal crossings	Interpolation routine	Logical or function Prints ATA and in-	Computes perturba- tive accelerations	Computes station coordinate quantities	Predicts rise and set times	Computes and prints elements Generates print times
CALLS SUBROUTINES		NTRP		XRAY	ATMMD, COORD, DFDB. FEQX, GRAV, TMATX	v tuli	TRAJG, XY2A, IXTUV	XY2A
CALLED BY SUBROUTINES	DFDB, INCN, INCN1, SACT	TRACK	CRASH, FILL, FITB, TRAJ, TRAJ3, TRAJG	INPUT	DAUX	CMPA, CMPE CMPRD	DESA	INITB CPPR TRAJ, TRAJ3 TSET2
NEGPHPDN	×	×	×	×	×		×	××
	×		×	×	×			×××
OX H Q H H	×		×	××	×	×		××
SECMENT NUMBER	62	23	62	63	03	15	16	12 22 13
NAME	NOB	NODE	NTRP	OR PATTY	PERT	PHI	PRDCT	PREL PRELM PRGEN

Table 15 (cont.)

	ROUTINE SIZE			262		C	1216		115		140		257		6	1233			77.1	T+/	10	0 -	70	135			456	
	FUNCTION			Prints partial	derivatives	Dummy routine	Prints trajec-	tory	Sets up station	codes	Sets up code list	for parameters	Converts spheri-	cal to cartesian	coordinates	Controls partial	and residual	computation	+ · · · · · · · · · · · · · · · · · · ·	restandi ourpur	Random number	Tallian III allian	generators	Recovers old	matrix from	tape		i ior thrusts and ' kicks
	CALLS SUBROUTINES			HUMAH2			CALD, SPEC,	XY2R, ITEST								SUMP, CMPA,	CMPRG, TCDE		CAPO, SIGMA								MATVEC	
	CALLED BY SUBROUTINES			CPPR		INITA	CPPR		TRAIN,	MNG	ACE		INCN,	TSET	TSET3	FITB			gu v a	NOW.	CATNR	DIM	EON	LEAST			TRAJ	TKAJ3
ZIO	A T A	: U	шz			×							×								Þ	4 1	×					
USED IN	A A L	<u>ы</u>	ထမ	×		×	×						×		-	_											×	-
O	M B C	ıы	H			×			×		×		×			×				<				×			×	_
	SEGMENT NUMBER			22	(03	22		01	1	01		62			15			ű	7	16	75	91	25			13	
_	NAME			PRXI	6	PSET	PTRAT		PUTPQ		QUEEN		R2XY			KAUK			דתו	TOWN	RDM	MTMUG	KULIN	RECVR			REINT	-

Table 15 (cont.)

	ROUTINE SIZE		540	153	153			250			630		103			103	224			125			317	244		233	
	FUNCTION		Same as REINT	Replaces word by	an integer	and ATA for	constraints	Modifies solu-	tion for	constraints	Checks for vehi-	cle visibility	Finds I, J ele-	ment of inverse	matrix	Same as RL1	Computes range	and range rate	for station N	Computes stored	quantities for	RADR	Sorts data	Corrects radar	parameters	Corrects trajec-	tory parameters
	CALLS SUBROUTINES										NTRP, WRKK,	IXIUV								STANG			CDX, BCDX	TCDE		NOB	
	CALLED BY SUBROUTINES		TRACK	CSCP, DUM	TRAIN	770		SLV			GAINB		RESTI			BABT	SITE			INITB			TRAIN	TEAST		LEAST	
NIO	A H A D	ыZ	×								×					×	×			×						_	
SED	E D B B B B B B B B B B B B B B B B B B	ж ы					_					_								×					4	- 1	
DIO.	民田口田	H	7	×		Κ		×					×							×	_		×	>			
	SEGMENT		23	01	ŭ	7		25			16	İ	25			90	. 90			12			11	33	25	32	1
	NAME		REINT2	REPL	E	VEST.		REST1			RIST		RLI			RL	RKDT			RSET			RSORT	0	SACK	TOVO	ONC

Table 15 (cont.)

ROUTINE SIZE	135	116	522	157	1	2443			204	07.0	0	137	770	007	237	i i
FUNCTION	Saves old matrix	Shuffles two data	Second difference editing routine	Dinde correct atoms		Decodes parameter	words for data)	Solves normal	ions	yrite special tra- jectory tape	Computes station	data	Interpolates for special trajectory	print times Codes data words	for each station
CALLS SUBROUTINES			IXTUV, DAPT			BABT, LUBS,	CMPN, WZKD,	ASPECT,		LEGSA					DCODE	SUMP, IXTUV
CALLED BY SUBROUTINES	LEAST	TRAJG TRAJ3,	ISEIZ TRAIN	A2XY, BADY,	ASPECI	GAINB			LEAST		MAINE, CPPR	KICS, PSET,	TRAIN	TRAJ3	KICS, RADR	FITB
NEGPHADEZ		×				×									×	
		×												×	×	-
USED O T B B A T T E P P E E	×	×	×	×					×			×			×	× -
SEGMENT	32	06	11	15		16			32		31	01		31	62	15
NAME	SAVEN	SHUFLE	SIFT	SIGMA		SITE			SLV		SPEC	STANG		STIR	SUMP	TBIAS

Table 15 (cont.)

	ROUTINE SIZE				217	101	227	236		1330					453		1010							
	FUNCTION				Same as TBIAS	Decodes date	Control routine for segment 01	Calculates T	matrix for variational	Control routine	for segment 11				Generates trajec-	tory tape for data	Controls integra-	tion in trajectory	prediction mode					
	CALLS SUBROUTINES				SUMP, IXTUV		INITB,			KICS, SIFT,	ACE, PUTPQ,	REPL, TROUT	TAIDLY,	STANG,			MOVE, MEP	APSIS,	KTIM, CPPR,	SHUFL,	STIR, DEQ2,	PRGEN,	CRASH,	TSET2 DXDA1
	CALLED BY SUBROUTINES				FITA	FILL, NAMER	MAINI	PERT		TINTB					GAINA		MATNE							
Z	DAH	A	G	ыZ		×					10220													
딥	O T D R B A T T	D	Ы	民日		×		×									>	<						
SI	0 K E	A	ы	Н	×	×	×	×		×					×									
	SEGMENT NUMBER				21	62	01	13		11					23		31	1						
	NAME				TBIAS1	TCDE	TINITB	TMATX		TRAIN				-	TRACK		TD A 13	COUNT						

Table 15 (cont.)

	ROUTINE SIZE				1033				267		,	152			1047		313			514		
	FUNCTION				Controls integra-	gration in orbit	מפרפו וווידוומרוס		Reads trajectory	from tape for	data generation	Computes yaw,	roll and pitch	corrections	Tracking data out- put routine		Tracking covari-	ance matrix set-	up and output routine	Initializes inte-	gration	
	CALLS SUBROUTINES						CRASH,	ALADD,	PRGEN, TRIM, NTRP.	SHUFLE					TCDE, EXIT,	 DJULA,	ALPHAG,	CANT		CSET, DXDA,	A2XY, XY2A, DXDRSR,	R2 XY
	CALLED BY SUBROUTINES				FITA				CATNR	PRDCT		TRAJG			TRAIN		E	TROOT		INITB		
N O		A		ыZ		<u>. </u>			>	4		×								×		
USED O T	⋈ 4	; b	Ь	저 되						_	_		_			 		.		×		
DO	24 14	<u> </u>	巨	H	×		_			_		_			×	 		×	-	×		
	SEGMENT	NOTIFIER	1		21				71	01		16)		11		,	11		12	1	
	NAME				TRAJ				C A G	1 KAJG		TRIM			TROUT			TROUTI		TSET		

Table 15 (cont.)

	ROUTINE SIZE		403		344		262			331					263		!	255	172				1	1/2	
	FUNCTION		Initializes inte- gration for orbit	determination	Initializes inte-	gration for tra-	jectory prediction Initializes inte-	gration for mul-	tiple vehicles	Initializes inte-	gration for data	generation	Computes unit	vector	Calculates matrix	for variational	equations	Writes header page	Controlled output	routine	Data generation	routine		Converts units of	ATA
	CALLS SUBROUTINES		DAUX, DEQ2, GRAV1,	PRGEN,	SHUFL DAUX, DEQ2,	MOVE, GRAV1	SHUFL R2XY, DXDRS			DAUX, DEQ2,	GRAV1,	MOVE2			MATMAT						CALD, IXTUV			HUMAH1	
	CALLED BY SUBROUTINES		FITA, TRAJ		MAINE,	TRAJ3	FITA			TRACK			TRAJ,	RADT	PERT			HNDL	RIST, SITE		GAINB,	TRAJG	SITE	PATTY	
NI O		a Z								×			×					×	×		×			_	
SED	民国口臣市民政党	द छ			_×			_					×									-		_ ×	
	SEGMENT NUMBER D	4	21 x		31		21			23			62 x		03 ×			16	16		16			32	
	NAME		TSET1		TSET2		TSET3			TSET4			UNVEC		VMATX			WHDR	WRKR	-	WZRD			XRAY	

Table 15 (cont.)

ROUTINE SIZE	412	225	3713	240	
FUNCTION	Converts rectangular coordinates	Converts rectangular coordinates	to spherical Output initial conditions and	constants Sets up sigmas for zero residuals	
CALLS				SUMP	
CALLED BY SUBROUTINES	DIFF, INCN, PRDCT	DIFF, INCN,	INCN1	TRAIN	
N D A H A D H Z	×	×	×		
HAAPAR	×	×	×		
USED O O T B B A A B T B B A B B A B B A B B B B B	×	×	×	×	
SEGMENT NUMBER	62	62	02	11	
NAME	XY2A	XY2R	YNTL	ZRRIT	

5.4 Variable Lists

In this section are listed several variable arrays used in the TRACE-D program. These particular variables were chosen because they are the most important and critical storage areas of TRACE-D. They contain all of the indicators and input that dictate the logical program flow.

Table 16. NUMB ARRAY

NUMB	NUMBER OF	SET	INPUT
_	RADAR STATIONS	INTAGT	NAME
2	OBSERVATION TIMES	TRAIN	
	STATIONS REQUIRING	DUM	
	OR STATIONS REQUIRING SIMULATION DATA	DUM	
m	WORDS IN COMPACTED RADAR OBSERVATION LIST - TOTAL	TRAIN	
7	WORDS OF COMPACTED RADAR OBSERVATIONS IN CORE NOW	TRAIN	
5	DIFFERENTIAL EQUATION PARAMETERS TO BE SOLVED FOR	CHAIN	
9	\vdash	CHAIN	
7	RADAR STATION PARAMETERS TO BE SOLVED FOR	KING	
_∞	RADAR OBSERVATION PARAMETERS TO BE SOLVED FOR	KING	
6	PROGRAM TAPE UNIT	CHAIN -	PTAPE
10	MAXIMUM ITERATIONS ALLOWED	CHAIN -	MAXIT
11	TOTAL PARAMETERS (SUM OF 5,6,7 AND 8)	TRAIN	
12	TRAJECTORY PARAMETERS (SUM OF 5 AND 6)	TRAIN	
13	OBSERVATIONS (TOTAL NUMBER OF MEASUREMENTS)	TRAIN	
14	PRESENT ITERATION		
15	BASIC TYPES OF OBSERVATIONS	CHAIN	
16	SIZE OF BUFFERS IN DEAN (Q DATA) - IF = 0, SET TO 5000	DEAN	
17	TOTAL RADAR PARAMETERS (SUM OF 7 AND 8)	TRAIN	
18	TAPE UNIT FOR PLANETARY COORDINATE TAPE	CHAIN -	CTAPE
19	SECOND ORDER DIFFERENTIAL EQUATIONS BEING INTEGRATED	INCN	
	(3*(1+NUMB(12)*IFLAG(8)))		
20	POSSIBLE KINDS OF RADAR PARAMETERS	CHAIN	
	(LAT, LONG, HEIGHT, AND BIASES)		
21	WORDS IN CORE FOR SIGHTING EPHEMERIS BUCKET	CHAIN	
22	POSSIBLE KINDS OF SIGHTING DATA	CHAIN	
23	DATA NOISE CONTROL (ZERO FOR NO NOISE, NON-ZERO STARTS	CHAIN -	NOISE
	RANDOM NUMBER GENERATORS FOR DATA NOISE)		
24	POSITION IN ITIN LIST OF FUNCTION BEING EXECUTED	ILIN	
25	EFFECTIVE PARAMETERS BEING SOLVED FOR	CHAIN -	KNST
)-(NO		
26	UNIT FOR	CHAIN -	ETAPE
	(IF ZEKU, NO LAFE GENERALED)		

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27	FLOCKS OF DATA	TRAIN	•
28	TAPE UNIT FOR ECLIPSE COORD TAPE	CHAIN	
29	CURRENT PASS THRU DUM - 0 FOR 1ST PASS, 1 FOR REST	CHAIN	
30	ELEMENTS IN ATA	MAIN	
31	TAPE UNIT FOR NOMINAL TRAJ. FOR DIFFERENCING RUN	INPAL -	- NTAPE
32	TAPE UNIT FOR DIFFERENCED TRAJ. FOR DIFFERENCING RUN	INPAL -	- DTAPE
	(LOGICAL NO.)		
33	MAXUMUM NUMBER OF 2ND DIFFERENCE EDITOR ITERATIONS		
34	NUMBER OF 3 COLUMN PARAMETERS		
35			
36			
37	NOT USED		
000			
39			
40			
42	CONVERSION CONSTANT FOR DISTANCES GENERATED IN GAIN.		
	MUST BE INPUT = 3443.9336 NM/ER OR 6975.246 KYD/ER		
43	LOGICAL TAPE NUMBER FOR ANOTHER COMPACTED DATA TAPE TO BE GENERATED IN TRAIN	TRAIN	
77	INDICATOR FOR FIXED BASELINE STATION LOCATION CONSTRAINTS		
	- 1 IF OPTION BEING USED		
45	NOT USED		
94		TTAPE	
47-50	NOT USED		

Table 17. IFLAG ARRAY

FLAG -	FLAG - OPTION INDICATORS	INPUT
1	CURRENT FUNCTION BEING EXECUTED = 1, $\left(\frac{1}{2}\right)$ ORBIT DETERMINATION = 2,	
	= 3, TRAJECTORY = 4, CAIN	
2	RESTORE (1) LAST GOOD SOLUTION OR CORRECT (0) PRESENT SOLUTION	
3		
4	REASON FOR EXIT FROM MAIN (1-MAXIMUM NUMBER OF ITERATIONS.	
	2-CONVERGED, 3-TRAJECTORY COMPLETED)	
2	F-7	
9		
	ALL E	
7	ZERO, REGULAR RESIDUAL PRINTING	
	NEGALIVE, AI ILEKATION = MAXII, SOKIED KESIDUALS AKE PKINIED	
	POSITIVE, AT ITERATION = MAXIT, ONLY SORTED RESIDUALS ARE	
	PRINTED. NO RESIDUALS ARE PRINTED PRIOR TO THIS.	
	USED ONLY WHEN RESIDUAL PRINTING INDICATED IN THE PRCDE. (PRCDE(2))	
8	ANALYTIC TRAJECTORY PARTIALS (0) OR VARIATIONAL EQUATIONS (1)	PARTL
6	BOUNDS PROVIDED FOR LEAST SQUARES SOLUTION (1) OR NO BOUNDS (0)	
10	NOT USED	
11	T-MATRIX OPTION IF=0, NO T-MATRIX	TMATX
	=1, INPUT DRHODH*H/RHO, NO EARTH FLATTENING	
	=2, INPUT DRHODH*H/RHO, USE EARTH FLATTENING	
	=3, CALC. DRHODH*H/RHO, NO EARTH FLATTENING	
	=4, CALC, DRHODH*H/RHO, USE EARTH FLATTENING	
12	PARAMETER SPECIFYING SEQUENCE OF FUNCTIONS TO BE	ILIN
13	PERFORMED	
14	USED IN GAIN. IF = 0, SORT OUTPUT NON-ZERO, DO NOT SORT	
	USED IN SUBROUTINE FINTR IN MAIN	
15	TRAJECTORY COMPARISON OPTION	IDIFF
	IF IDIFF = 0, REGULAR TRAJECTORY	
	1,	
	= 2, IST COMPARISON, DIFFERENCES WRITTEN ON DIAPE	

= 3, OTHER THAN FIRST OR LAST COMPARISON CASES = 4, FOR ONE AND ONLY COMPARISON CASE = 5, LAST COMPARISON	FORTRAN LOGICAL UNIT FOR TRAJECTORY TAPE WRITTEN BY FIT A AND GAIN A.	SET NON-ZERO IN TSET IF TO IS A PARAMETER	NON-ZERO, ACCUMULATE ATA IN DOUBLE PRECISION	(FOR ATA LESS THAN 2746)	IF SET NON-ZERO SIGMA TABLE WEIGHTING VALUES WILL BE USED EVEN IF	VARIANCE/COVARIANCE MATRICES ARE INCLUDED IN DATA DECK	IF NON-ZERO, OPERATE IN 3 PTS./PASS MODE	OPTION INDICATOR FOR 2ND DIFFERENCE EDITOR, CONTROLS EDITING OF	FIRST 2 AND LAST 2 POINTS		NOT USED		SET IN TSET IF ALPHA PARTIALS ARE TO BE COMPUTED.	AFTER COMPLETING FIT A CALL FIT B (0) OR DO NEXT FUNCTION (1).	NOT USED	INDICATOR FOR RESPECIFICATION OF GEOPOTENTIAL COEFFICIENTS	Ø = RESPECIFICATION	NUMBER OF ORBIT ADJUSTS IN SPECIAL TABLE (DELV)
---	--	---	--	--------------------------	---	--	--	---	---------------------------	--	----------	--	---	--	----------	--	---------------------	---

IDLV

Table 18. CNDT ARRAY

CNDT - PARAMETER LIST. CODES ARE IN ITRCD

1-6	INITIAL CONDITIONS
7	T-ZER0
80	CDA/W
6	GM
10-18	J2-J10
19-38	J21-J66 ORDERED J21, J31, J41,,J56, J66
39-58	LAMBDA21-LAMBDA66 SAME
59	ASUBE ' EARTH RADIUS
09	OMEGASUBA - ATMOSPHERE ROTATION RATE
61	Il THRUST (T1*EXPF(-T2*T)
62	T2
68-75	
80-87	TO, AND
92-99	AND DRAG FOR SATELLITE
104-111	
116-123	TO, AND DRAG FOR
124-129	
130-135 \	NOT USED
136-153	
154	K-ZERO TELEMETRY DATA
155	K-ONE TELEMETRY DATA

Table 19. KIND ARRAY

Table 20. TREG ARRAY

USE OF TREG FOR INTEGRATION (COW)

```
CURRENT TIME IN MINUTES FROM MIDNIGHT OF EPOCH
                                                                  CURRENT INTEGRATION STEP SIZE
                                NEQ (SET IN COW AT B = 35)
                                                                                                                                                                   X-DBL. DOT(PI)
                                                                                                                                                 X-DBL. DOT
                                                                                                                                  X-DOT(PI)
CONTENTS
                                                                                                                  X-DOT
                                                                                                  X(PI)
                                                                                                                                                  (K-2NEQ)-(K-2NEQ-2)
(K-2NEQ-31)-(K-2NEQ-31-2)
                                                                                                                                  (K-NEQ-31)-(K-NEQ-31-2)
                                                                                                                 (K-NEQ)-(K-NEQ-2)
                                                                                                 (K-3I)-(K-3I-2)
TREG CELL
                                                                                (K)-(K-2)
                                                                 (K+1)
                                (K+3)
                                                (K+2)
```

WHERE --- NEQ = 3(N+1)

K = L-3 (CURRENTLY = 5490)
L = DIMENSION OF TREG = 90(M+1)+3
M = MAXIMUM NUMBER OF I.C. AND D.E.

= TOTAL NUMBER OF I.C. AND D. E. PARAMETERS FOR THE CURRENT RUN

MAXIMUM NUMBER OF I.C. AND D.E. PARAMETERS (CURRENTLY = 60)

USE OF TEMP FOR INTEGRATION (DAUX AND PERT)

/4																	GRAV CALLING SEQUENCE	GRAV CALLING SEQUENCE	GRAV CALLING SEQUENCE	GRAV CALLING SEQUENCE	CALLING		GRAV CALLING SEQUENCE	GRAV CALLING SEQUENCE	GRAV CALLING SEQUENCE	GRAV CALLING SEQUENCE	GRAV CALLING SEOUENCE	GRAV CALLING SEQUENCE	GRAV CALLING SEQUENCE	CALLING	CALLING	GRAV CALLING SEQUENCE
OSE OF TEN FOR INIBORALION (DAGA AND FERT)	E	×	PSI(P1)	PSI (PK)	DELTA-T	X-DOT	PSI-DOT(P1)	PSI-DOT(PK)	X-DOUBLE DOT	PSI-DOUBLE DOT(P1)	PSI-DOUBLE DOT(PK)		X,	R**2	R**3	R**5	ж	SIN(PHI)	COS(PHI)	SIN(ALPHA(G))	COS(ALPHA(G))	SIN(ALPHA)	COS (ALPHA)	F(1)	GLH	ROT MATRIX	U POTENTIAL	А	В	υ	D	ы
מסו מד דרווי דלוו	(1)	(2)-(4)	(5)-(7)	(3K+2)-(3K+4)	(185)	(186)-(188)	(189)-(191)	(3K+186)-(3K+188)		(372) - (374)	(3K+369)-(3K+371)	(552)	(553)	(554)	(555)	(556)	(557)	(558)	(559)	(260)	(561)	(562)	(563)	(564–566)	(567–569)	(570–578)	(579)	(580–588)	(589–608)	(609–628)	(629–637)	(638–657)

185.

SEOUENCE	SEQUENCE																												
SRAV CALLING	GRAV CALLING																												55
GRAV	GRAV																												BODIES
_														_															F OTHER
SIN(M(LAMBDA-LAMBDA(MN)))	COS (M(LAMBDA-LAMBDA(MN)))	DFDX(1) V-MATRIX	DFDX(2) T-MATRIX	DFDXD U-MATRIX	DF/DX*(PSI(PK))	DF/DXDOT*(PSI-DOT(PK))	DF/DB	RHO (DENSITY)	(VEL OF SOUND)	(ALTITUDE)		(MACH NUMBER)	X-DOT(A)	D/V(A) = RHO/2*V(A)*CDA/W	F(3)	ABSF(X-DOT) = V(A)	F(4) THRUST FORCE	ABSF(X(J))**3	ABSF(X-X(J))	BSF(X-X(J))**3	ABSF(X-X(J))**5	X-X(1)	x-x(2)	X-X(3)	(4) X-X	x-x(5)	(9) X-X	F(2)	INTERPOLATED VELOCITIES OF OTHER BODIES
S	Ö	Q	D	D	D	D	Q	R	A	H		X	×	D	[- -1	A	Œ	A	A	A	A	×	×	×	×	×	×	Ĭ.	Ħ
(658-677)	(678-697)	(902-869)	(707-715)	(716-724)	(725-727)	(728-730)	(731-910)	(916)	(917)	(818)	(616)	(650)	(921-923)	(954)	(925-927)	(828)	(935-937)	(938-943)	(676-776)	(950-955)	(956-961)	(967-964)	(865-967)	(026-896)	(971-973)	(926-526)	(617-919)	(980-982)	(983-1000)

STAT--PROPERTIES RELATED TO THE LTH STATION

UNITS (RADIANS) (RADIANS) (EARTH RADII)	(EARTH RADII) (EARTH RADII)
DESCRIPTION GEODETIC LATITUDE EAST LONGITUDE ALTITUDE COS (LAT)	SIN (LAT) W1 W3 SIGMA SET REFRACTIVITY TYPE STATION NAME Q STATION NUMBER P STATION UNMBER
CELL (1,L) (2,L) (3,1) (4,L)	(5,L) (6,L) (7,L) (8,L) (9,L) (10,L)

Table 23. COMMON LAYOUT

COMPON A - BLOCKS NEEDED FOR ALL LINKS - 8722 CELLS

₹	H.		LIEMP	45
AU	S	-	ITRCD	62
O	v	100	KIND	10
8		3.6	NUMB	20
පි		56	PARINT	20
C		56	PKICK	50
ຮ	DT	160	PRTIM	21
දි	RAM	2	PUSH	200
DA	VE	100	REFR	15
DP	RAM	. 07	SIS	1
DR	AG .	120	SUSP	1
딥	-1	20	TRAJX	367
FI	ن ن	10	TRUNI	552
FL	33	100	TUMP	100
H	(A)	24	XTRA	50
Ħ	TAPE	17	TEMP	1000
IF	LAG	30	TREG	5493

COMMON B - BLOCKS NEEDED FOR FIT AND DATA GENERATION LINKS - 4300 CELLS

				00	
100	200	100	100	11,100	
BIAS	PRAM	IGGY	SIGMY	TAT	
<u>Д</u>	84	S	S	S	
1800	100	100	100	200	100
OK	IAS	PAR	ICDIC	PRCD	SIG
Ģ	E	Д	H	I	H

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13. ABSTRACT						

This report describes the MITRE version of the TRACE-D program now in operation. While the primary function of TRACE-D is orbit determination, options are also available in the program for trajectory prediction and observational data generation. A functional description of these features is contained in this report along with a complete user's

manual and a brief program description.

Security Classification LINK A LINK B LINK C KEY WORDS ROLE ROLE WT ROLE **PROGRAMMING** ORBIT DETERMINATION TRAJECTORY PREDICTION OBSERVATIONAL DATA GENERATION SATELLITE TRACKING